

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool Basin Dakota Formation Dakota County San Juan  
Initial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 10-13-64  
Company PAN AMERICAN PETROLEUM CORP. Lease Gallegos Canyon Unit-Dak. Well No. 176  
Unit 6 Sec. 23 Twp. 28N Rge. 13W Purchaser \_\_\_\_\_  
Casing 4-1/2 Wt. 10.9 I.D. 4.032 Set at 6402 Perf. 6313-6330 To \_\_\_\_\_  
Tubing 2-3/8 Wt. 4.7 I.D. 1.993 Set at 6272 Perf. 6241 To 6235  
Gas Pay: From 6246 To 6330 L 6200 xG .700 -GL 4401 Bar.Press. 12  
Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well Single  
Date of Completion: 10-6-64 Packer None Single-Bradenhead-G. G. or G.O. Dual  
Reservoir Temp. \_\_\_\_\_

## OBSERVED DATA

Tested Through PROVER (Choke) PROVERType Taps Flange

| No. | Flow Data   |              |             |                      |           | Tubing Data |           | Casing Data |           | Duration of Flow Hr. |
|-----|-------------|--------------|-------------|----------------------|-----------|-------------|-----------|-------------|-----------|----------------------|
|     | (Line) Size | (Choke) Size | Press. psig | Diff. h <sub>w</sub> | Temp. °F. | Press. psig | Temp. °F. | Press. psig | Temp. °F. |                      |
| 1.  | 9 Days      |              |             |                      |           |             |           |             |           |                      |
| 2.  | 2 inch      | .730         | 461         |                      |           | 461         | 600° sat. | 979         | 900° sat. | 3 hr.                |
| 3.  |             |              |             |                      |           |             |           |             |           |                      |
| 4.  |             |              |             |                      |           |             |           |             |           |                      |
| 5.  |             |              |             |                      |           |             |           |             |           |                      |

## FLOW CALCULATIONS

| No. | Coefficient (24-Hour) | $\sqrt{h_{wpf}}$ | Pressure psia | Flow Temp. Factor F <sub>t</sub> | Gravity Factor F <sub>g</sub> | Compress. Factor F <sub>pv</sub> | Rate of Flow Q-MCFPD @ 15.025 psia |
|-----|-----------------------|------------------|---------------|----------------------------------|-------------------------------|----------------------------------|------------------------------------|
| 1.  | 12.2690               |                  | 473           | 1.000                            | .9230                         | 1.040                            | 3740                               |
| 2.  |                       |                  |               |                                  |                               |                                  |                                    |
| 3.  |                       |                  |               |                                  |                               |                                  |                                    |
| 4.  |                       |                  |               |                                  |                               |                                  |                                    |
| 5.  |                       |                  |               |                                  |                               |                                  |                                    |

## PRESSURE CALCULATIONS

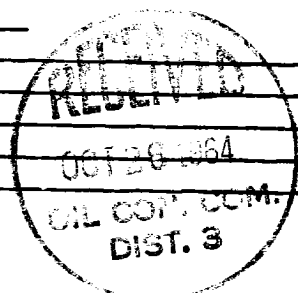
Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
F<sub>c</sub> \_\_\_\_\_ (1-e<sup>-s</sup>)

Specific Gravity Separator Gas \_\_\_\_\_  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 2076 P<sub>c</sub> 4,300,776

| No. | P <sub>w</sub> P <sub>t</sub> (psia) | P <sub>t</sub> <sup>2</sup> | F <sub>c</sub> Q | (F <sub>c</sub> Q) <sup>2</sup> | (F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> ) | P <sub>w</sub> <sup>2</sup> | P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup> | Cal. P <sub>w</sub> | P <sub>w</sub> /P <sub>c</sub> |
|-----|--------------------------------------|-----------------------------|------------------|---------------------------------|--|-----------------------------|--|---------------------|--------------------------------|
| 1.  |                                      |                             |                  |                                 |  | 962,001                     | 3327,095   |                     |                                |
| 2.  |                                      |                             |                  |                                 |  |                             |  |                     |                                |
| 3.  |                                      |                             |                  |                                 |  |                             |  |                     |                                |
| 4.  |                                      |                             |                  |                                 |  |                             |  |                     |                                |
| 5.  |                                      |                             |                  |                                 |  |                             |  |                     |                                |

Absolute Potential: 6940 MCFPD; n .73COMPANY PAN AMERICAN PETROLEUM CORPORATIONADDRESS Box 400, Farmington, New MexicoAGENT and TITLE F. L. Hubers, District EngineerWITNESSED By: Original Signed By:COMPANY G. W. EATON, JR.

REMARKS



## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressability factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .