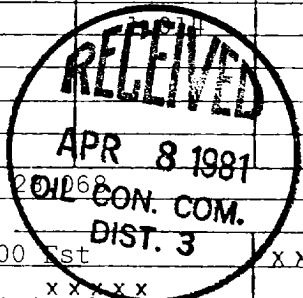


MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 4-3-81	
Company ARCO Oil & Gas Company, Division of Atlantic Richfield		Connection None	
Pool Basin Dakota		Formation Dakota	
Completion Date 3-24-81	Total Depth 6550	Plug Back TD 6528	Elevation 6024
Farm or Lease Name Krause WN Federal		Well No. 7E	
Coq. Size 4 1/2	Wt. 10.5#	d 4.052	Set At 6549
Perforations: From 6432 To 6514		Well No. 7E	
Tiq. Size 2 3/8"	Wt. 4.7#	d 1.995	Set At 6386
Perforations: From To		Unit Sec. Twp. R10W J 32 28N 11W	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single Gas		Packer Set At None	
Producing Thru Tubing		Baro. Press. - P <sub>g</sub> 12.0	
Reservoir Temp. *F #		Mean Annual Temp. *F	
State New Mexico		County San Juan	
L 5109	H 5109	G <sub>g</sub> .800 Est	% CO <sub>2</sub> % N <sub>2</sub> % H <sub>2</sub> S
Prover 2"		Meter Run Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Size	X	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.		Temp. *F
SI							1117		1117		SI 10 Days
1.	2"		.750"	95		62	177		465		Flow 3 Hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow O, Mcfd
1	9.453		107	.9981	1.118		1144
2.							
3.							
4.							
5.							



NO.	P <sub>r</sub>	Temp. *R	T <sub>r</sub>	Z	Gas Liquid Hydrocarbon Ratio	Mcf/tbl.
1	.16	522	1.23	.973	A.P.I. Gravity of Liquid Hydrocarbons Specific Gravity Separator Gas .800 Est Specific Gravity Flowing Fluid X X X X X	XXXXXX
2.					Critical Pressure 665 P.S.I.A.	
3.					Critical Temperature 424 R	
4.						
5.						

NO.	P <sub>c</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	(1) $\frac{P_c^2}{P_w^2} = 1.0595$	(2) $\left[\frac{P_c^2}{P_w^2}\right]^n = 1.0443$
1	35721	268	71585	1203056		
2.						
3.						
4.						
5.						

AOF = Q  $\left[\frac{P_c^2}{P_w^2} - 1\right]^n = 1195$

Absolute Open Flow 1195 Mcfd @ 15.025 Angle of Slope @ .75 Slope, n .75

Remarks: Well tested thru 48/64" choke

Approved by Division	Conducted by Rex Hitchcock	Calculated by Rex Hitchcock	Checked by
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