

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12-31-74	
Company Northwest Pipeline Corp.				Connection New Completion			
Pool Basin				Formation Dakota		Unit San Juan 29-6	
Completion Date 12-24-74		Total Depth 8100		Plug Back TD 8052		Elevation 6822	
Farm or Lease Name San Juan 29-6 Unit							
Csg. Size 4.500	Wt. 10.5 & 11.6	d 4.052	Set At 8084'	Perforations: From 7882 To 8016		Well No. 106	
Tbg. Size 1.900	Wt. 2.9	d 1.610	Set At 8013	Perforations: From To		Unit Sec. Twp. Rge. M 13 29 6	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Gas Single				Packer Set At none		County Rio Arriba	
Producing Thru casing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a 12.0	
State New Mexico							
L	H	G _g 0.585	% CO ₂	% N ₂	% H ₂ S	Prover 3/4"THC	Meter Run Taps

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2503		2510		7 day SI
1.			.750	279#		60°	456				3 hr
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		291	1.000	1.012	1.021	3,718
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ X X X X X X X X Specific Gravity Flowing Fluid _____ X X X X X Critical Pressure _____ P.S.I.A. _____ P.S.I.A. Critical Temperature _____ R _____ R			
1.								
2.								
3.								
4.								
5.								

P _c 2522 P _c ² 6360,484			
NO.	P _r ²	P _w	P _w ²
1		468	219,024
2			
3			
4			
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{6,360,484}{6,141,460}$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0266$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3,817$$

Absolute Open Flow	3,817	Mcfd @ 15.025	Angle of Slope ϕ	Slope, n	75
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Remarks: Well produced heavy fog of H₂O throughout test.

Approved By Commission:	Conducted By: Larry Moore	Calculated By: Bobby Broughton	Checked By: REF
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