

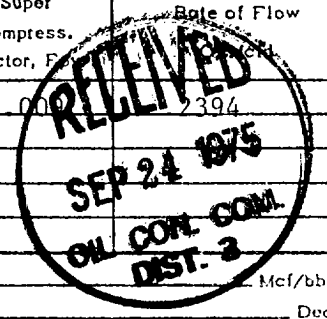
**NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test <input type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 9/22/75		
Company Northwest Pipeline Corporation			Connection New Completion			
Pool Blanco			Formation Mesa Verde		Unit San Juan 29-6	
Completion Date Sept 14, 1975		Total Depth 5766		Plug Back TD 5732	Elevation 6484	
Csg. Size 4.500		Wt. 10.5	d 4.052	Set At 5766	Perforations: From 5130 To 5720	
Tbg. Size 2.875		Wt. 4.7	d 1.995	Set At 5693	Perforations: From To	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Gas-single				Packer Set At None		
Producing Thru Tubing		Reservoir Temp. °F @	Mean Annual Temp. °F	Baro. Press. - P _a 12.2		
L	H	G _g .69	% CO ₂	% N ₂	% H ₂ S	
				Prover Orifice Meter	Meter Run 4"	Taps Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Meter p.s.i.g.	Diff. Meter	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	4 X 2.500		61			62°	284		519		3hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	Meter Differential	Pressure Meter Static	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{sc}	Rate of Flow
1.	103.00	7.1	2.7	.998	1.204	1.00	2394
2.							
3.							
4.							
5.							



NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

F _c 801	P _c ² 641601					
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{641601}{359640}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.5436$
1.		531	281961	359640		
2.						
3.						
4.						
5.						

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3695$

Absolute Open Flow	3695	Mcf @ 15.025	Angle of Slope θ	Slope, n	.75
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Remarks: _____

Approved By Commission:	Conducted By: Fred W. Farnick	Calculated By:	Checked By:
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