

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 12-3-75	
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Company Northwest Pipeline Corp.		Connection New Completion		
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Pool Blanco		Formation Mesa Verde		Unit S.J. 29-6
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Completion Date 11-24-75		Total Depth 5810		Plug Back TD 5776		Elevation 6409 GR		Farm or Lease Name S.J. 29-6 Unit	
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Csg. Size 4.500		Int. d 10.5		Set At 4.052		Set At 5810		Perforations: From 5178 To 5630		Well No. 1A	
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Tq. Size 2.375		Int. d 4.7		Set At 1.995		Set At 5604		Perforations: From To		Unit Sec. Twp. Hgt. P 3 29 6	
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Type Well - Single - Broadhead - G.C. or G.O. Multiple Gas - Single						Packer Set At none		County Rio Arriba			
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Producing thru Tubing		Reservoir Temp. °F ρ		Mean Annual Temp. °F		Baro. Press. - P _a 12.0		State New Mexico			
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L		H		G _g .670		% CO ₂		% N ₂		% H ₂ S		Prover orifice meter		Meter Run 4"		Taps flange	
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FLOW DATA						TUBING DATA			CASING DATA		Duration of 8 Day
NO.	Prover Line Size	X	Orifice Size	Meter p.s.i.g.	Diff.	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							574		574		SIP
1.	4 x 2.50		60	6.5	60		265		460		3 hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	Differential Meter	Pressure Meter Static	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow 8 day O. Mcd
1	103.21	6.5	2.7	1.000	1.222	1.030	2280
2.							
3.							
4.							
5.							

NO. P _r Temp. °R		DEF 3 273		Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.							
1.		OIL TEMP. 100		A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.							
2.		INST 3		Specific Gravity Separator Gas _____ X X X X X X X X X X							
3.		3		Specific Gravity Flowing Fluid _____ X X X X X							
4.		4		Critical Pressure _____ P.S.I.A. _____ P.S.I.A.							
5.		5		Critical Temperature _____ R _____ R							

P _c 586 P _w 343396		NO. P _r ² P _w ² P _c ² - P _w ²		(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.8471$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.1918$	
1		472 222784 120612		AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4,997$			
2							
3							
4							
5							

Absolute Open Flow 4997 Mcd @ 15.025		Angle of Slope θ _____		Slope, n .75	
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Remarks: Diff. from L-10 chart. Coefficient from chart factor 3.162 + orifice factor 32.64. Variable choke set @ 48/64. Well produced approx 1/2 bbls of condensate.

Approved By Commission:		Conducted By: Fred Hamrick		Calculated By: Bobby Broughton		Checked By: 	
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