

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test:		☒ Initial		☐ Annual		☐ Special		Test Date: 6-30-78			
Company				Connection							
Northwest Pipeline Corp.				New Well							
Pool				Formation				Unit			
Blanco				Mesa Verde				San Juan 29-6			
Completion Date		Total Depth		Plug Back TD		Elevation		Farm or Lease Name			
6-19-78		5975		5937		6049		San Juan 29-6 Unit			
Csg. Size	Wt.	d	Set At	Perforations:		Well No.					
7.00	20.0	6.456	3852	From 5379 To 5887		38A					
4.500	10.5	4.052	3687-5972								
Tbg. Size	Wt.	d	Set At	Perforations:		Unit Sec. Twp. Rge.					
2.375	4.6	1.995	5868	From To		D 16 29 6					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple						Packer Set At		County			
Gas-Single						None		Rio Arriba			
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Base. Press. - P _e		State			
Tubing		@		60		12.0		New Mexico			
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover Positive Choke		Meter Run		Taps	
		.671									

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							832		955		SIP
1.	2 X .750			329		60	329		817		3 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	9.604		341	1.000	1.221	1.037	4147
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.	
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	
2.					Specific Gravity Separator Gas _____ X X X X X X X X	
3.					Specific Gravity Flowing Fluid _____ X X X X X	
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.	
5.					Critical Temperature _____ R _____ R	

P _c 967	P _c ² 935089		
NO.	P _t ²	P _w	P _w ²
1		829	687241
2			
3			
4			
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.7728$		$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.7071$	
ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 11,226$			

Absolute Open Flow	11,226	Mcf @ 15.0 PS	Angle of Slope @	Slope, n	.75
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Remarks: Well Produced a trace of condensate.			
Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Fred Hamrick	B.J. Broughton	