

Form C-122
Revised 5-1-65

Type Test		☒ Initial		☐ Annual		☐ Special		Test Date		10-3-79	
Company				Connection							
Southland Royalty Company				Northwest Pipeline Corporation							
Pool				Formation				Unit			
Gobernador				Pictured Cliffs							
Completion Date		Total Depth		Plug Back TD		Elevation		Farm or Lease Name			
9-26-79		6079'		6000'		6634' GR		Creek			
Csg. Size		Wt.		d		Set At		Perforations:		Well No.	
7.000		23#		6.366		3855'		From 3452' To 3658'		1-A	
4.500		10.50#		4.052		3718-6075'					
Tbg. Size		Wt.		d		Set At		Perforations:		Unit Sec. Twp. Rge.	
1.900		2.76#		1.610		3639'		From --- To ---		P 4 29N 5W	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple						Packer Set At		County			
G. G. Multiple						3765'		Rio Arriba			
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a		State			
Tbg		8				12.2		New Mexico			
L		H		Gg		% CO ₂		% N ₂		% H ₂ S	
				.700						Prover	
										Meter Run	
										Taps	
FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1134		1132		
1.	2"		3/4"				192		648		3 hrs
2.											
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mc/d				
1	12.365		204.2	1.0000	.9258	1.0000	2338				
2.											
3.											
4.											
5.											
NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mc/d/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____		X X X X X X X X				
3.					Specific Gravity Flowing Fluid _____		X X X X X				
4.					Critical Pressure _____ P.S.I.A.		P.S.I.A.				
5.					Critical Temperature _____ R		R				
P_c 1146.2 P_c^2 1,313,774											
NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.4965$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4087$				
1		660.2	435,864	877,910							
2											
3											
4											
5											
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3293$											
Absolute Open Flow 3293						Mc/d @ 15.025		Angle of Slope @		Slope, n 85	
Remarks: Dry											
Approved By Commission:				Conducted By: Leroy Castleman				Calculated By: James Smith			
								Checked By:			