

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form O-122  
Revised 9-1-67

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 8-18-78							
Company Southland Royalty Company			Connection Not Dedicated								
Pool Blanco			Formation Mesaverde		Unit						
Completion Date 7-29-78		Total Depth 6168'	Plug Back TD 5986'	Elevation 6586' GR	Form or Lease Name Carson						
Cr. Size 4.980	Wt. 10.38#	d 4.052	Set At 3632-3780'	Perforations: From 5577' To 5898'							
Trg. Size 2.375	Wt. 4.7#	d 1.995	Set At 5866'	Perforations: From To							
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single				Facker Set At ---							
Producing Thru Tbg		Reservoir Temp. *F P	Mean Annual Temp. *F	Baro. Press. - P <sub>a</sub> 12.2	State New Mexico						
L	H	G <sub>g</sub> .700	% CO <sub>2</sub>	% N <sub>2</sub>	% H <sub>2</sub> S						
		Prover	Meter Run	Taps							
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	Temp. *F	Duration of Flow
1.	2"		3/4"				1232		1225		1 hr
2.							150		374		2 hrs
3.							110		270		3 hrs
4.							96		260		
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super. Compress. Factor, F <sub>pv</sub>	Rate of Flow O. Mcfd				
1	12.365		108.2	-1.0000	0.9258	1.0000	1,239				
2.											
3.											
4.											
5.											
NO.	P <sub>i</sub>	Temp. *R	T <sub>i</sub>	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____ X X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X						
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ R _____ R						
$P_c = 1244.2$ $P_w = 1,548,034$											
NO.	P <sub>i</sub>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0503$	(2) $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0375$					
1		272.2	74,093	1,473,941							
2					AOP = Q $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1,285$						
3											
4											
5											
Absolute Open Flow				1,285	Mcf @ 15.025		Angle of Slope $\theta$		.75		
Remarks:											
Approved By Commission			Conducted By Dwayne Horton			Calculated By L. O. Van Ryan			Checked By <i>[Signature]</i>		