

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test		☒ Initial		☐ Annual		☐ Special		Test Date		11/1/83	
Company						Connection					
Northwest Pipeline Corporation						New Completion					
Basin						Formation					
						Dakota					
Completion Date				Total Depth		Plug Back TD		Elevation		Form or Lease Name	
10/9/83				8308'		8290'		6499' KB		San Juan 30-5 Unit	
Coq. Size	Wt.	d	Set At	Perforations:				Well No.			
4.500	11.6	4.052	8308	From 8215' To 8260'				#101			
Trg. Size	Wt.	d	Set At	Perforations:				Unit Sec. Twp. Rge.			
2.375	4.7	1.995	8290'	From To				A 35 30 5			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple						Packer Set At		County			
Gas - Single						None		Rio Arriba			
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a		State			
Tubing		A				12.0		New Mexico			
L	H	Gg Est.	% CO ₂	% N ₂	% H ₂ S	Positive Choke		Meter Run		Taps	
		.590									

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Flow Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	SIP						2890		2890		
1.	2"	X	.750"			64°	105	64°	397	64°	3 Hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	9.604		117	.996	1.302	1.010	1472
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.	
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	
2.					Specific Gravity Separator Gas _____ X X X X X X X X	
3.					Specific Gravity Flowing Fluid _____ X X X X X	
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.	
5.					Critical Temperature _____ R _____ R	

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1		409	167281	8265935
2				
3				
4				
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.0202$$

$$ACF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1494$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0151$$

Absolute Open Flow	1494	Mcf/d @ 15.025	Angle of Slope, θ		Slope, n	.75
--------------------	------	----------------	-------------------	--	----------	-----

Remarks: Produced light mist throughout test. Vented 220 MCF.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	George Bryan	M.J. Turnbaugh	