## Revised 12-1-55

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool	l <u>Basin Dakota</u>			_Formation	Dak	Dakota		CountySan_Juan		
	tial X Annual_							דרתוו	<del>-</del>	
Company TEXACO Inc. Lease St. of New Mex. Keys Well No. 1										
	<u> </u>									
Casi	ng 4.5 W	t. 9.5	O_I.D	4,09 Se	t at 64	77Per	rs. 62	79	To	6410
Tubing 2-3/8 Wt. 4.7 I.D. 1.99 Set						at 6350 Perf. 635			To	Open End
Gas Pay: From 6279 To 6410 L xGGL Bar. Press										
Prod	ucing Thru:	Casin	rg	Tu	ıbi.ng	X	Type We	ll Singl	e Gas	O Dual
Producing Thru: Casing Tubing X Type Well Single Gas  Single-Bradenhead-G. G. or G.O. Dual  Date of Completion: 5-14-63 Packer Reservoir Temp.										
	•					ED DATA				
Test	ed Through	(PXXXVE)	Chok	e) (XMEXXXX)	Ķ			Туре Тар	s	
Flow Data						Tubing Data			ata	I
No.	(Prover) (Line)	(Choke	Pre	ss. Diff.	Temp.		-		Temp.	of Flow
	Size	Size	ps	ig h <sub>w</sub>	°F.	psig	°F.	psig	°F.	Hr.
SI						2058	020	2070	ļ	7 days
1. 2.	2	•75	<u> </u>		<del> </del>	415	860	1014	<del> </del>	3 hours
3.										
4.									<del>                                     </del>	<u> </u>
5.					<u> </u>	<u> </u>		l	J	<u> </u>
					FLOW CAL	CULATION	5	10		Data of Flour
No.	Coefficient Pressure F					ow Temp. Gravity Compress. Rate of Flow Factor Factor Factor Factor F <sub>pv</sub> P <sub>pv</sub> Q-MCFPD 9 15.025 psia				
NO.	(24-Hou	$r) \sqrt{h_{w}p_{f}}$		psia		t	Fg	F <sub>pv</sub> 9 15.025 psia		● 15.025 psia
1.	12.365			427	.9777		.9258	1.045		4.994
2.										<del></del>
3.			<del></del>	<u> </u>						
4. 5.										
						Calculatio				
Gas Liquid Hydrocarbon Ratiocf/bbl. Specific Gravity Separator Gas700  Gravity of Liquid Hydrocarbonsdeg. Specific Gravity Flowing Fluid  F_c(1-e^{-8}) P_c_2082 P_c^24.334.724										
· c			(			-	C——	<del></del>		
No.	P <sub>w</sub>	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	2 (1	( <sub>0</sub> ) <sup>2</sup>	P.,2	P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	Ca	al. Pw
NO.	Pt (psia)	¹t	rc*	(1°C-4)	i) (i	(cQ) <sup>2</sup> L-e <sup>-s</sup> )	••		1	$\frac{P_{\mathbf{W}}}{P_{\mathbf{C}}}$
1.						1	.052.67	6 3.282	048	
3.		<del></del>	<del>                                     </del>	<del></del>						
1. 2. 3. 4. 5.										
			<b></b>					<u> </u>		
	lute Potent		6,15	3	MCFPD;	, n	75			
ADDR	PANY TE	XACO I	x 810.	Farming	ton, Ne	w Mexic	0 00			
AGEN	ESS P.	dan	id K	Celli	e_	Dist	Sain.	run	74.	
	ESSED_ PANY					<del></del>	<del></del>	FRE	<u> </u>	
JOHN					PF	MARKS			1	\
					TUESE	CANAL			كة -	<b>\</b>

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ( $P_{\rm W}$ ). MCF/da. @ 15.025 psia and 60° F.
- $P_c$  72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- $P_w$  Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- $F_g$ : Gravity correction factor.
- $F_{t}$  Flowing temperature correction factor.
- FpvI Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\mathbf{W}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{W}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .