## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

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Pool	. Un	design	ted	Fc	rmation	Dako	te		County	8	na Juna
Init	ial										
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Unit	F	ec. <b>3</b> 4	ጥພ	291	Ros	13	Pur	chaser			
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	ng 2 3/8 W										
	Pay: From			_							
Data	ucing Thru: of Complet	ion.	3/1k/	/60	Poolsos	. <b>B</b> o	Si	ngle-Brad	enhead-G. (	or G	.O. Dual
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io.	(Line)	(Orifi	Lce)			-				-	of Flow
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+	12.3550	<del></del>	V W	1	57	1.000	-	0.960	1.031		11/45
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					PRE	ESSURE C	ALCULAT:	IONS			
s L	iquid Hydro	carbon	Ratio	D		cf/bbl.		Speci	ific Gravit	v Sena	rator Gas
	ty of Liqui		carb	ons_		deg.		Spec	ific Gravit	y Flow	ing Fluid
			(:	l-e <sup>-s</sup> ∑				Pc 20	<del>55</del>	$P_c^2$	<b>23.025</b>
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٠.		$P_{\mathbf{t}}^2$	F,	e	$(F_cQ)^2$	(F	cQ) <sup>2</sup> -e-s)	$P_w^2$	$P_c^2 - P_w^2$	Ca	Pw Pc
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MAR 2 2 1960 OIL CON. COM. DIST. 3

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ( $P_{\rm W}$ ). MCF/da. @ 15.025 psia and 60° F.
- P<sub>c</sub>I 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw- Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If  $P_{\rm W}$  cannot be taken because of manner of completion or condition of well, then  $P_{\rm W}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\rm t}$ .

