Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised	12-1-55

1.   2.   3   3   4   526	Pool	ol Undesignated Formation Daketa C									County_	San	Juan	· · · · · · · · · · · · · · · · · · ·		
Unit A Sec. 32 Twp. 29% Rge. 11W Purchaser  Casing 44 Wt. 9.5 a I.D. Set at 6300 Perf. 6044 To 6230  Tubing 2-16 Wt. 4.5 I.D. Set at 6300 Perf. 6210 To 6213  Gas Pay: From 6044 To 6230 L. xG .460 -GL Bar.Press.  Producing Thru: Casing Tubing X Type Well Single-Chardenhead-G. G. or G.O. Dual Reservoir Temp.  OBSERVED DATA  Tested Through (Choke) (Press.) Diff. Temp. Press. Temp. Press. Temp. Press. Temp. Of Flow Size Pick (Orifice) Page Phys. Diff. Temp. Press. Temp. Pr	Initi	ial		Annual				Speci	al	X	I	Date of	Te <b>st</b> _	5-17·	-60	
Casing   Wit   Min   M										We]	ll No.	A				
Casing   Wit   Min   M	Unit		Sec <b>32</b>	Twp	29 H	<u> </u>	ge	11W	Pur	chaser						
Tubing 2-1/8 Wt. 1.6 I.D. Set at 6318 Perf. 6219 To 6219  Cas Pay: From 6044 To 6230 L xG 4600 -GL Bar.Press.  Producing Thru: Casing Tubing I Type Well  Single-Bradenhead-G. G. or G.O. Dual  Reservoir Temp.  OBSERVED DATA  Tested Through (Choke) (Press. Diff. Temp. Press. Temp. Press. Temp. Of Flow Size Size psig h, Op. psig Op. psig Op. psig Op. Hr.  SIL 1. 2130		_											_	6230		
Gas Pay: From 6044 To 6230 L xG .460 _GL Bar.Press.  Producing Thru: Casing Tubing I Type Well Single-Gas  Date of Completion: 4-25-60 Packer Single-Bradenhead-G. G. or G.O. Dual Reservoir Temp.  OBSERVED DATA  Tested Through (Choke) (Prover) (Prov												1				
Producing Thru:   Casing																
Date of Completion:   4-25-60   Packer   Single-Bradenhead-G. G. or G.O. Dual Reservoir   Temp.																
Choke   Chok									Si	nøle-Rrad	lent	ead_C	G. or	G.O.	Dual	
Type Taps		•											<del></del>		<del></del>	
Flow Data	Teste	d Through	(2000	<b>≖</b> ) (Cha	ke)	(Marketon )		OBIC V B.	D DAIR		т	me Tan	\ <b>C</b>			
Prover   Choke   Orifice   Size   Press   Diff   Temp.   Press   Temp.   Press   Temp.   Duration of Flow   Size   Size   psig   h_w   O_F.   psig   O_F.   psig   O_F.   psig   O_F.   Press   Temp.   Duration of Flow   Size   Size   psig   h_w   O_F.   psig   O_F.						\r			Tubin	- Doto				<del></del> -		
Size   Size   psig   hw   OF, psig   OF, p	No		(Chok	e) Pr		Diff.	Te	mp.			_			.		
1.	140 .				sig	h <sub>w</sub>	o	F.	psig	°F.		psig	<sup>⊃</sup> F.			
2.	SI								2120			23.20				
Flow CALCULATIONS   Flow Temp.   Gravity   Compress.   Rate of Flow Temp.   Factor   Garatic   Factor   Facto	2.					<u> </u>				<del></del>	+	<del> </del>		+		
Flow Calculations	3.		3/4	5	26		7	0				1247			hre	
Pressure   Flow Calculations   Flow Temp.   Gravity   Factor   F	4.	<del></del>	<del> </del>							<del> </del>	+	<u> </u>				
Coefficient	2. !		<del></del>		1	<del></del>	L	L		٠		<u> </u>			<del> </del>	
No. (24-Hour)			<del></del>		<b></b>							<b>.</b>				
(24-Hour)	No	Coeffici	ent		Pre	essure			*					•		
1.		(24-Hour) 7/h.ps			١,	psia F <sub>4</sub>				Factor F-		11			•	
12.3650   538   5905   9393   1.061   6567	1.		· + *	M <sub>T</sub> T	+			- 0			-	- p <b>v</b>			,,,,, pol	
12.3650   538   5905   9393   1.061   6567	2.				<del> </del>					<del></del>						
PRESSURE CALCULATIONS  as Liquid Hydrocarbon Ratio cf/bbl. Specific Gravity Separator Gas Specific Gravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid Pc	3。	12.3650				538	وم	7905		9393		1.06		656	7	
PRESSURE CALCULATIONS  as Liquid Hydrocarbon Ratio cf/bbl. Specific Gravity Separator Gas Specific Gravity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid Pc	4.	<del></del>			<del> </del>					<del></del>	_	ļ				
as Liquid Hydrocarbon Ratio cf/bbl. Specific Gravity Separator Gas Specific Gravity Flowing Fluid P <sub>c</sub> 2112 P <sub>c</sub> 4444  No. P <sub>w</sub> P <sub>t</sub> (psia) P <sub>t</sub> F <sub>c</sub> Q (F <sub>c</sub> Q) <sup>2</sup> (F <sub>c</sub> Q) <sup>2</sup> (F <sub>c</sub> Q) <sup>2</sup> P <sub>w</sub> P <sub>c</sub> P <sub>c</sub> P <sub>w</sub> P <sub>c</sub> P <sub>c</sub> P <sub>w</sub> P <sub>c</sub> P <sub>c</sub> P <sub>c</sub> P <sub>w</sub> P <sub>c</sub> P <sub>c</sub> P <sub>c</sub> P <sub>w</sub> P <sub>c</sub>	<u> </u>	<del></del>		<del></del> -	Ь.											
Pw		PRESSURE CALCULATIONS														
Pw	og Tignid Urdreverhan Dekin															
C																
No.   P <sub>W</sub>   P <sub>t</sub>   F <sub>c</sub> Q   (F <sub>c</sub> Q) <sup>2</sup>   (F <sub>c</sub> Q) <sup>2</sup>   P <sub>w</sub> 2   P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>   Cal.   P <sub>W</sub>   P <sub>c</sub>   P <sub>c</sub>																
No. Pt (psia) Pt FcQ (FcQ)2 (FcQ)2 Pw2 Pc-Pw Cal. Pw Pc Pc Pc Pw Pc Pc Pw Pc Pc Pc Pw Pc										Ç—			- 0			
No. Pt (psia) Pt FcQ (FcQ)2 (FcQ)2 Pw2 Pc-Pw Cal. Pw Pc Pc Pc Pw Pc Pc Pw Pc Pc Pc Pw Pc		<u> </u>		г —		<del></del> -			<del></del>		γ	<del> </del>	<del></del>	<del></del>		
Absolute Pouential: 9062 MCFPD; n .75 1.389  COMPANY Redfern & Herd, Inc. ADDRESS Box 1747, Midland, Texas  AGENT and TITLE T. A. Dugan, Cassulting Engineer  WITNESSED  COMPANY REMARKS	No.	<b>"</b>	$P_{t}^2$	F <sub>C</sub> Q		$(F_cQ)^2$		(F <sub>C</sub> Q	$(2)^2$	P <sub>10</sub> 2		$P_c^2 - P_w^2$	C.	al.	P <sub>w</sub>	
Absolute Potential: 9062 MCFPD; n75 1.389  COMPANY Redfern & Herd, Inc. ADDRESS Box 1747, Midland, Toms AGENT and TITLE T. A. Dugan, Consulting Engineer WITNESSED COMPANY  REMARKS		t (psia)						(1 <u>-</u> e	-s)	w			] :	P <sub>w</sub>	P <sub>c</sub>	
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AGENT and TITLE T. A. Dugan, Compulting Engineer WITNESSED COMPANY REMARKS								·								
COMPANY REMARKS			Box 174	7. Mid	and,	Terns	W	ne	·			<del> </del>			<del></del>	
REMARKS	WITNES	SED		- ATTENDED	VOL	HAT FIELD			<del></del>			<del> </del>		-	—. — ——	
	COMPAN	Y														
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## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log-log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q  $\equiv$  Actual rate of flow at end of flow period at W. H. working pressure (P<sub>W</sub>). MCF/da. @ 15.025 psia and 60° F.
- $P_c$  72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw. Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- $h_{\mathbf{w}}$  Differential meter pressure, inches water.
- Fg Gravity correction factor.
- $F_t$  Flowing temperature correction factor.
- F<sub>DV</sub> Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\rm W}$  cannot be taken because of manner of completion or condition of well, then  $P_{\rm W}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\rm t}$ .

