MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Poo	1	eia Del	eta .	Fc	rmation		Debote	<u> </u>	_County_	See	Juan
Ini	tial	K	Anni	ual		Spec	ial		_Date of	Test	12-30-64
Com	pany PAN A	MR ICAI	PETRO	LEDK COL	D.	Lease 🖦	lleges G	ayon Uni	k-Dek Wel	.1 No	188
Uni	t 3	_Sec	30 Tv	√p	Rg	e. 120	Purc	haser			
Cas	ing 4-1/2	Wt1	10.5	I.D. 4.0	52 Se	t at	Ol Pe	57. rf. 58	32-44 10-20	То	5834-43
Tub	ing 2-3/8	Wt	4.7	.D. 1.9	95 _Se	t at	749 Pe	rf	3712	To	5718
Gas Pay: From 5732 To 5643 L 5788 xG .760 -GL 4652 Bar.Press. 12											
Producing Thru: Casing Tubing Type Well											
Producing Thru: Casing Tubing Type Well Single Bate of Completion: Packer Packer Reservoir Temp.											
OBSERVED DATA											
Tested Through (Choke) (Choke) (Heter) Type Taps											
Flow Data Tubing Data Casing Data											
	(Trover	7 (C			Diff.	Temp.		Temp.		Temp.	Duration
No.	(Line) Size		Size	nsig	h	o _F	nsiø	o _F	psig	1 1	of Flow Hr.
SI				Pore	W		2011		2005		
1.	2 Inch			399			399	60° 66€.	384	60° 68	. 3 18.
2 . 3•				 				 		-	
4.											
5.				<u> </u>				<u> </u>		J	
FLOW CALCULATIONS											
No.	Coefficient (24-Hour) $\sqrt{h_{\eta}}$		Pressure		Flow	Flow Temp. Gravit		Compress. Rate of G-MCFI			
NO.			$\sqrt{h_{k}}$	hwpf psi		F.	t	F	Fnv		0 15.025 psia
1.	12.3	650)		421	1:00		.9256	1,031		4945
2.											
3。 4.			+								···
5.											
					PRI	ESSURE C	ALCUI ATI	ONS			
		_									
Gas Liquid Hydrocarbon Ratiocf/bbl. Specific Gravity Separator Gas Gravity of Liquid Hydrocarbonsdeg. Specific Gravity Flowing Fluid For a continuous formula for the continuous for the continuous formula for the continuous for the continuous formula for the continuous formula for the continuous for the continuous formula for the continuous for the continuous formula for the continuous formula for the continuous formula for the continuous formula for the continuous for the continuous formula for the continuous formula for the continuous for the continuous formula for the continuous formula for the continuous formula for the continuous for											
			((1-e ^{-s})				P _c	1700	P _c ²	110,000
	$P_{\mathbf{w}}$		2		,		.2		2 2		
No.	Pt (psia		$P_{\mathbf{t}}^2 \mid F$	CQ	$(F_cQ)^2$	(F	_c Q) ² -e ^{-s})	$P_{\mathbf{w}}^2$	$P_c^2 - P_w^2$	Ca	l. Pw Pc
1.	rt (psia	'				(1.	-6 -)	i 5,856	3,744, 144	P.	w 1°C
2.											
3. 4.										-OF	
5.										6F17	W.
Abso	olute Pore	ntial		3590		MCFPD:	n	.75		KLUL	I V Line
COMPANY											
	RESS	LE	3- A	AL SIGNED L W. Foell	striet i)IL COI	V. COM
	NESSED		YXIGIA F	AL SIGNED L	3Y					DIS'	
	PANY			TOSI		Direc	ADKC				
						₩.M.	w m 🛰				

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (P_W) . MCF/da. @ 15.025 psia and 60° F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- FgI Gravity correction factor.
- F_{t} Flowing temperature correction factor.
- F_{pv} Supercompressability factor.
- n I Slope of back pressure curve.

Note: If P_W cannot be taken because of manner of completion or condition of well, then P_W must be calculated by adding the pressure drop due to friction within the flow string to P_t .