MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

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## Sec. 37 Tem. 29N Rge. 10M Purchaser Southern Union Ques Co. 15ing. 51° Mt. 15.5 I.D. 1.950 Set at 1918 Perf. 1815 To 1880 Doing 11° Wt. 2.1 I.D. 1.25 Set at 1810 Perf. 1810 To 1825 Set 277 From 1815 To 1880 L 1825 xG 0.67 Est. GL 1222.7 Bar. Press. Coducing Thru: Casing Tubing Y Type Mell G. 0 Tem. OBSERVED DATA ### Type Mell G. 0 Tem. OBSERVED DATA Completion: Fab. 1, 1959 Facker 1712 Tubing Data Casing Data (Prover) (Choke) (Neber) Tubing Data Casing Data (Prover) (Choke) Press. Diff. Temp. Press. Temp. Press. Temp. Description: Size Size psig hw Op. psig CF. psig Pr. 1129 She 129 She 120 S	
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July December	
olute Potential: MCFPD; n 0.85	
RESS SOUTHERN UNION GAS COMPANY	
NT and TITLE Gilbert Feland, Jr. Asst. Drilling Superintendent	
REMARKS	
Paso Natural Gas Company, Box 997 Farmington, New Mexico REMARKS OIL CON 1959 OST. CON,	
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INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa ře.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q \equiv Actual rate of flow at end of flow period at W. H. working pressure (P_W). MCF/da. @ 15.025 psia and 60° F.
- P_c 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If P_{W} cannot be taken because of manner of completion or condition of well, then P_{W} must be calculated by adding the pressure drop due to friction within the flow string to P_{t} .

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