

NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Basin Dakota Formation Dakota County San Juan
Initial 1 Annual _____ Special _____ Date of Test 4-17-64
Company PAN AMERICAN PETROLEUM CORP. Lease Gallegos Canyon Unit-Dak. Well No. 133
Unit B Sec. 20 Twp. 20N Rge. 12W Purchaser _____
Casing 4-1/2 Wt. 10.5 I.D. 4.032 Set at 6021 Perf. 3043-33/3023 To 3041/3047-33
Tubing 2-3/8 Wt. 4.7 I.D. 1.995 Set at 3030 Perf. 3021 To 3027
Gas Pay: From 3043 To 3023 L 3030 xG .700 -GL 4120 Bar.Press. 12
Producing Thru: Casing _____ Tubing 1 Type Well Single
Single-Bradenhead-G. G. or G.O. Dual
Date of Completion: 4-10-64 Packer None Reservoir Temp. _____

OBSERVED DATA

Tested Through (Flange) (Choke) (Flange) Type Taps Flange

| No. | Flow Data | | | | Tubing Data | | Casing Data | | Duration of Flow Hr. |
|-----|-------------|--------------|-------------|----------------------|-------------|-------------|-------------|-------------|----------------------|
| | (Line) Size | (Choke) Size | Press. psig | Diff. h _w | Temp. °F. | Press. psig | Temp. °F. | Press. psig | Temp. °F. |
| 1. | 7 Days | | | | | | | | |
| 2. | 2 inch | .730 | 671 | | | 671 | 67° est. | 1401 | 67° est. |
| 3. | | | | | | | | | |
| 4. | | | | | | | | | |
| 5. | | | | | | | | | |

FLOW CALCULATIONS

| No. | Coefficient (24-Hour) | $\sqrt{h_{wpf}}$ | Pressure psia | Flow Temp. Factor F _t | Gravity Factor F _g | Compress. Factor F _{pv} | Rate of Flow Q-MCFPD @ 15.025 psia |
|-----|-----------------------|------------------|---------------|----------------------------------|-------------------------------|----------------------------------|------------------------------------|
| 1. | 11.3630 | | 671 | 1.000 | .9238 | 1.006 | 8342 |
| 2. | | | | | | | |
| 3. | | | | | | | |
| 4. | | | | | | | |
| 5. | | | | | | | |

PRESSURE CALCULATIONS

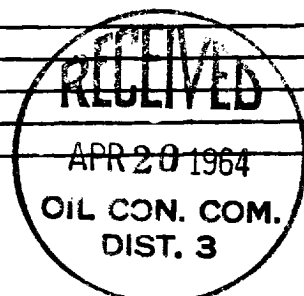
Gas Liquid Hydrocarbon Ratio _____ cf/bbl.
Gravity of Liquid Hydrocarbons _____ deg.
F_c _____ (1-e^{-s})

Specific Gravity Separator Gas _____
Specific Gravity Flowing Fluid _____
P_c 2117 P_c 4,461,690

| No. | $\frac{P_w}{P_t}$ (psia) | P _t ² | F _c Q | (F _c Q) ² | $\frac{(F_c Q)^2}{(1-e^{-s})}$ | P _w ² | P _c ² -P _w ² | Cal. P _w | $\frac{P_w}{P_c}$ |
|-----|--------------------------|-----------------------------|------------------|---------------------------------|--------------------------------|-----------------------------|--|---------------------|-------------------|
| 1. | | | | | | 1,996,309 | 1,403,120 | | |
| 2. | | | | | | | | | |
| 3. | | | | | | | | | |
| 4. | | | | | | | | | |
| 5. | | | | | | | | | |

Absolute Potential: 12,901 MCFPD; n .73
COMPANY PAN AMERICAN PETROLEUM CORPORATION
ADDRESS Box 400, Farmington, New Mexico
AGENT and TITLE P. L. Roberts, District Engineer
WITNESSED [Signature]
COMPANY _____

REMARKS



INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w).
MCF/da. @ 15.025 psia and 60° F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
psia
- P_w = Static wellhead working pressure as determined at the end of flow period.
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if
flowing through casing.) psia
- P_f = Meter pressure, psia.
- h_w = Differential meter pressure, inches water.
- F_g = Gravity correction factor.
- F_t = Flowing temperature correction factor.
- F_{pv} = Supercompressability factor.
- n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .