

NEW MEXICO OIL CONSERVATION COMMISSION  
GAS WELL TEST DATA SHEET - - SAN JUAN BASIN

(TO BE USED FOR FRUITLAND, PICTURED CLIFFS, MESAVERDE, & ALL DAKOTA  
EXCEPT BARKER DOME STORAGE AREA)

Pool ACTON-PICTURED CLIFFS Formation PICTURED CLIFFS County SAN JUAN  
Purchasing Pipeline EL PASO NATURAL GAS COMPANY Date Test Filed OCTOBER 6, 1956  
Operator STANDARD OIL & GAS COMPANY Lease LEWIS GAS UNIT '90' Well No. 1  
Unit P Sec. 26 Twp. 20N Rge. 10W Pay Zone: From 2096 To 2100  
Casing: OD 5 1/2" WT. 21.0 Set At 2070 Tubing: OD 2 1/2" WT. 2.10 T. Perf. 2096  
Produced Through: Casing ^ Tubing 1 Gas Gravity: Measured ^ Estimated .45  
Date of Flow Test: From 9/28/56 To 9/29/56 \* Date S.I.P. Measured 9/29/56  
Meter Run Size 4" Orifice Size 2.35 Type Chart P.S.M. Type Taps 1

OBSERVED DATA

Flowing casing pressure (Dwt) \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (a)  
Flowing tubing pressure (Dwt) \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (b)  
Flowing meter pressure (Dwt) \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (c)  
Flowing meter pressure (meter reading when Dwt. measurement taken):  
Normal chart reading \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (d)  
Square root chart reading ( \_\_\_\_\_ ) <sup>2</sup> x spring constant \_\_\_\_\_ = \_\_\_\_\_ psia (d)  
Meter error (c) - (d) or (d) - (c) \_\_\_\_\_ ± \_\_\_\_\_ = \_\_\_\_\_ psi (e)  
Friction loss, Flowing column to meter:  
(b) - (c) Flow through tubing: (a) - (c) Flow through casing \_\_\_\_\_ = \_\_\_\_\_ psi (f)  
Seven day average static meter pressure (from meter chart):  
Normal chart average reading \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (g)  
Square root chart average reading ( \_\_\_\_\_ ) <sup>2</sup> x sp. const. \_\_\_\_\_ = \_\_\_\_\_ psia (g)  
Corrected seven day avge. meter press. (p<sub>f</sub>) (g) + (e) \_\_\_\_\_ = \_\_\_\_\_ psia (h)  
P<sub>t</sub> = (h) + (f) \_\_\_\_\_ = \_\_\_\_\_ psia (i)  
Wellhead casing shut-in pressure (Dwt) \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (j)  
Wellhead tubing shut-in pressure (Dwt) \_\_\_\_\_ psig + 12 = \_\_\_\_\_ psia (k)  
P<sub>c</sub> = (j) or (k) whichever well flowed through \_\_\_\_\_ = \_\_\_\_\_ psia (l)  
Flowing Temp. (Meter Run) \_\_\_\_\_ °F + 460 \_\_\_\_\_ = \_\_\_\_\_ °Abs (m)  
P<sub>d</sub> = 1/2 P<sub>c</sub> = 1/2 (l) \_\_\_\_\_ = \_\_\_\_\_ psia (n)

FLOW RATE CALCULATION

Q = \_\_\_\_\_ X  $\left( \frac{\sqrt{(c)}}{\sqrt{(d)}} = \frac{\text{_____}}{\text{_____}} = \text{_____} \right)^* = \text{_____}$  MCF/da  
(integrated)

DELIVERABILITY CALCULATION

D = Q .472  $\left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} = \frac{21.97}{22.94} \right]^n \cdot \text{_____} = \text{_____}$  MCF/da.

SUMMARY

P<sub>c</sub> = 21.97 psia  
Q = .472 Mcf/day  
P<sub>w</sub> = 22.94 psia  
P<sub>d</sub> = 22.94 psia  
D = .472 Mcf/day

Company Standard Oil and Gas Company  
By L. E. Bower, Jr. (LMB)  
Title Field Engineer  
Witnessed by \_\_\_\_\_  
Company \_\_\_\_\_

- \* This is date of completion test.
- \* Meter error correction factor

REMARKS OR FRICTION CALCULATIONS

GL	(1-e <sup>-S</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-S</sup> ) R <sup>2</sup>	P <sub>t</sub> <sup>2</sup> (Column i)	P <sub>t</sub> <sup>2</sup> + R <sup>2</sup>	P <sub>w</sub>
<u>2100</u>	<u>.405</u>	<u>231.5</u>	<u>11.97</u>	<u>21.97</u>	<u>64.36</u>	<u>22.97</u>



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