## NEW MEXICO OIL CONSERVATION COMMISSION One-point Back Pressure Test for Gas Wells (Deliverability)

Form C-122-C 4-1-54

·	signated	Fo	rmation_	Point L	ookout	Cou	nt <del>y</del>	San Juan		·
Tnitial		Annual		_Special		Dat	e of tes	t1 <u></u>	9-57	
Company Su	nray Mid-	-Continent	011 Co.	Lease N.M.	Feder	ol min	م المسادمة	Wel	1 No1	<del></del>
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ໄລຣາກອ 🖰	1/2 Wt.	اندا الأحداث	). <i>L</i> .YO	Set at _592	U•	rer	11493		To	<u> </u>
ubing $2$	3/8 Wt	<u>.4•0</u> _ 1•1	2512	Set at <u>350</u> L <u>3500</u>	×	Per	T •	2260	Pan Pro	es 13 2
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$p_{\mathbf{f}}$	h <sub>w</sub>	Vp <sub>f</sub> h <sub>w</sub>	icient	Fg	Ft		Fpv	<u> </u>	<b>~</b>	
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LO-9-57	AM	10=12=5'							1 -	
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	2:00 PM		2:00 P	4	sary)	<del>/ or</del>	V 25 195 CON. CO		818	psia
	2:00 PM		2:00 P	4	sary)	<del>/ or</del>	CON. CO	P = -	<b>818</b> 89 <b>8</b>	psia _MCF/Da.
	2:00 PM	RICTION CA	2:00 Pi	MS(if necess	sary)	<del>/ or</del>	CON. CO	P = -	<b>818</b> 89 <b>8</b>	psia _MCF/Da
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°w389	2100 PM	DELIVERA  Pc  1+ Pw Pc 1	ABILITY C.	NS(if necess  ALCULATIONS $ \begin{array}{c c} P_{w} + P_{c} \\ \hline  & P_{c} \end{array} $	$\frac{\partial^2 \mathbf{c}}{\partial \mathbf{c}} = \mathbf{N}$	1203	CON. CO	P =	81.8 598 385 655 455	psia _MCF/Daa psia psia _MCF/Da
Pw	2100 PM	DELIVERA  Pc  1+ Pw Pc 1	ABILITY C.	NS(if necess  ALCULATIONS $ \begin{array}{c c} P_{w} + P_{c} \\ \hline  & P_{c} \end{array} $	$\frac{\partial^2 \mathbf{c}}{\partial \mathbf{c}} = \mathbf{N}$	1203	CON. CO	P =	81.8 89.8 38.5 65.5	psia _MCF/Daa psia psia _MCF/Da
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P <sub>w</sub> 389	2100 PM F1	DELIVER  Pc  1+ Pw Pc Log	ABILITY C.	ALCULATIONS $ \frac{P_{\mathbf{W}} + P_{\mathbf{C}}}{1 + \frac{P_{\mathbf{W}}}{P_{\mathbf{C}}}} \left(1 + \frac{P_{\mathbf{W}}}{P_{\mathbf{C}}}\right) $	$\frac{\partial^2 \mathbf{c}}{\partial \mathbf{c}} = \mathbf{N}$	1203	CON. CO	Pw =Pd =	81.8 598 385 655 455	psia _MCF/Da, psia psia _MCF/Da
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P <sub>w</sub>	2100 PM F1 5 -46 Sunray Mi Box 128,	DELIVERA  Pc  1+ Pw Pc  Log  d-Contine  Hobbs, Ne	ABILITY CASES 9.642-1	NS(if necess  ALCULATIONS $ \frac{P_{W} + P_{C}}{1 - \frac{P_{W}}{P_{C}}} \left(1 + \frac{1}{1}\right) $ The pany	$\frac{\partial^2 \mathbf{c}}{\partial \mathbf{c}} = \mathbf{N}$	1203	78	P = - P = -	818 898 385 655 455	psia _MCF/Da, psia psia _MCF/Da.
P <sub>w</sub>	2100 PM F 5 -53 -46 Sunray Mi Box 128, TITLE	DELIVER  Pc  1+ Pw Pc Lo  d-Contine  Hobbs Ar	ABILITY CASES Superi	ALCULATIONS $ \begin{array}{c c} P_{\mathbf{w}} + P_{\mathbf{c}} \\ \hline P_{\mathbf{c}} \\$	$\frac{\partial^2 \mathbf{c}}{\partial \mathbf{c}} = \mathbf{N}$	1203	78 Lo	P = - P = -	818 898 385 655 455 1.7.5 2.953	psia _MCF/Da, psia psia _MCF/Da.

This form is to be used for reporting deliverability tests in the designated Dry Gas Pools of Lea County as ordered by New Mexico Oil Conservation Commission Directive dated March 15, 1954, which directive was provided for by Orders R-365-A through R-376-A. For details regarding this test please refer to the above mentioned Directive.

## NOMENCLATURE

- Q = Actual flow at end of flow period at W. H. working pressure (P<sub>W</sub>). MCF/da. @ 15.025 psia and 60° F.
- P<sub>c</sub> = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- $P_d$  = Deliverability pressure; 80 % of 72 hour individual wellhead shutin pressure  $(P_c)$ . psia
- P = Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing). psia
- D = Deliverability at Deliverability pressure (P<sub>d</sub>) MCF/da. © 15.025 psia and 60° F.
- p, = Static meter pressure, psia.
- hw = Differential meter pressure, inches water CONSERVATION COMMISSION

 $F_{\sigma} = Gravity$  correction factor.

AZTEC DISTRICT OFFICE

Ft = Flowing temperature correction factor.

DISTRIBUTION NO.

F = Supercompressability factor.

n = Slope of back pressure curve.

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DELIVERABILITY FORMULA

State Land Office

D = Q	Γ		.36	
	1 -	Pc	1+	P <sub>w</sub>

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Note:	If Pw cannot be taken because of man	ner of completion or
	condition of well, then Pw must be c	alculated by adding
	the pressure drop due to friction wi	thin the flow string
	to P <sub>t</sub> .	