

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 2-8-77			
Company R&G Drilling Company				Connection Waiting on Pipeline					
Pool Fulcher Kutz				Formation Pictured Cliffs				Unit	
Completion Date 1-15-77		Total Depth 1970'		Plug Back TD 1885'		Elevation 5717'KB		Farm or Lease Name Hardie	
Csg. Size 4.500	Wt. 10.50	d 4.052	Set At 1931'	Perforations: From 1773' To 1851'		Well No. 62			
Thg. Size 1.660	Wt. 2.40	d 1.380	Set At 1791'	Perforations: From 1788' To 1791'		Unit P	Sec. 14	Twp. 29N	Rge. 12W
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single				Packer Set At none		County San Juan			
Producing Thru tubing		Reservoir Temp. °F 90 @ 1970		Mean Annual Temp. °F ----		Baro. Press. - P _a 12.0		State New Mexico	
L 1791	H 1791	Gg 0.650	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							265		265		7 day
1.	3/4" T.H.C.						20	60	210		3 hour
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		32	1.0000	0.9608	1.0000	380
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ XXXXXXXXXX
3.					Specific Gravity Flowing Fluid _____ XXXXXX
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 277	P _c ² 76,729				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	
1		222	49,284	27,445	
2					
3					
4					
5					

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 2.7957$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 911$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.3961$$

Absolute Open Flow	911	Mcf/d @ 15.025	Angle of Slope	0.85
Remarks:				

Approved By Commission:	Conducted By: Len Cunningham	Calculated By: Ewell N. Walsh	Checked By:
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ONE POINT BACK PRESSURE TEST

February 8, , 1977

OPERATOR R&G Drilling Company

LEASE Hardie WELL NO. 62

ID-1	Slope	0.85
	Baro. Press. .	12.00
	Choke Coeff.	12.3650
ID-2	Flow Temperature Factor	1.0000
ID-3	Specific Gravity Factor	0.9608
ID-4	Super compressibility Factor	1.0000
ID-5	Pc-Highest S.I.P. psig	265.
ID-6	Pw-Csg(Flow Tbg) , -Tbg(Flow Csg) psig	210.
ID-7	Choke press. -Tbg(Flow Tbg) -Csg(Flow Csg) , psig	20.
	Pressure, Pm	32.
	Rate of Flow, Q	380.
	Pc	277.
	Pc^2	76729.
	Pw	222.
	Pw^2	49284.
	$Pc^2 - Pw^2$	27445.
	$Pc^2 / Pc^2 - Pw^2$	2.7957
	$(Pc^2 / Pc^2 - Pw^2)^n$	2.3961
	Absolute Open Flow	911.