

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 3-17-78				
Company Getty Oil Company					Connection Not Connected				
Pool Bloomfield					Formation Shinarump				
Completion Date 7-27-73			Total Depth 4550'		Plug Back TD 4476'		Elevation 5618'		Farm or Lease Name W. Hanley "A"
Csg. Size 7.000	Wt. 23.0	d 6.370	Set At 3200	Perforations: From 3020 To 3030		Well No. 1			
Tbg. Size 1.750	Wt. 2.90	d 1.610	Set At 3013	Perforations: From Open ended		Unit Sec. Twp. Rge. F 18 29N 10W			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Is					Packer Set At -		County San Juan		
Producing Thru Tubing		Reservoir Temp. °F 8		Mean Annual Temp. °F 12		Baro. Press. - P _a 12		State New Mexico	
L 3013	H 3013	Gg .660	% CO ₂	% N ₂	% H ₂ S	Prover 2.000	Meter Run	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	14 dy SI						1079		1079		
1.	2.000	x	.750				51		346		1 hr.
2.	2.000	x	.750				31		263		2 hr.
3.	2.000	x	.750				23		239		3 hr.
4.											
5.											

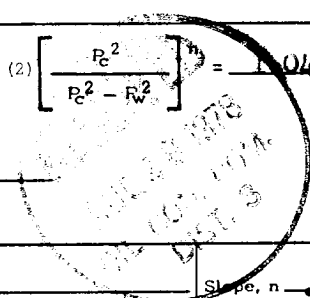
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.00		63	1.000	1.31	1.007	559
2	11.00		43	1.000	1.31	1.004	535
3	11.00		40	1.000	1.31	1.004	544
4.							
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1091	P _c ² 1190231			
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	1600	251	63001	1127230
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.0559}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.0415}$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{567}$



Absolute Open Flow 567	Mcf @ 15.025	Angle of Slope θ _____	Slope, n .75
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Remarks: **This OF was run in conjunction with the second half of the required Initial Packer Leakage Test, this being the upper zone. The lower zone is No. Verne**

Approved By Commission:	Conducted By: Dave Bouvier	Calculated By: Paul D Bernhost	Checked By:
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