

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☐ Initial ☐ Annual ☐ Special						Test Date <u>7-21-73</u>													
Company <u>Getty Oil Company</u>				Connection <u>at Junction</u>															
Pool <u>Bloomfield 1 Zone</u>				Formation <u>at Junction</u>		Unit													
Completion Date <u>7-20-71</u>		Total Depth <u>3315'</u>		Plug Back TD <u>3261'</u>		Elevation <u>5321'</u>													
Farm or Lease Name <u>Gett</u>		Well No. <u>1</u>		Perforations: From <u>3261'</u> To <u>3251'</u>		Unit Sec. Twp. Rge.													
Csg. Size <u>4.5 ID</u>	Wt. <u>9.5</u>	d <u>4.00</u>	Set At <u>3315'</u>	Perforations: From <u>3261'</u> To <u>3251'</u>		Unit Sec. Twp. Rge.													
Tbg. Size <u>1.900</u>	Wt. <u>2.40</u>	d <u>1.610</u>	Set At <u>3261'</u>	Packer Set At <u>3251'</u>		County <u>12</u> <u>27</u> <u>11</u>													
Type Well - Single - Brdhead - G.G. or G.O. Multiple				Packer Set At <u>3251'</u>		County <u>12</u> <u>27</u> <u>11</u>													
Producing Thru <u>3251'</u>		Reservoir Temp. °F <u>60</u>		Mean Annual Temp. °F <u>60</u>		Baro. Press. - P _a <u>12</u>													
State <u>Pa</u>		Prover <u>3251</u>		Meter Rpt <u>3251</u>		Taps <u>3251</u>													
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>L</td> <td>H</td> <td>Gq</td> <td>% CO₂</td> <td>% N₂</td> <td>% H₂S</td> </tr> <tr> <td><u>3251</u></td> <td><u>3251</u></td> <td><u>3251</u></td> <td></td> <td></td> <td></td> </tr> </table>				L	H	Gq	% CO ₂	% N ₂	% H ₂ S	<u>3251</u>	<u>3251</u>	<u>3251</u>							
L	H	Gq	% CO ₂	% N ₂	% H ₂ S														
<u>3251</u>	<u>3251</u>	<u>3251</u>																	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
1.	<u>2.000</u>	<u>x</u>	<u>.750</u>				<u>102</u>		<u>102</u>	
2.	<u>2.000</u>	<u>x</u>	<u>.750</u>				<u>31</u>		<u>127</u>	
3.	<u>2.000</u>	<u>x</u>	<u>.750</u>				<u>10</u>		<u>157</u>	
4.	<u>2.000</u>	<u>x</u>	<u>.750</u>				<u>5</u>		<u>1</u>	
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.	<u>11.00</u>		<u>12</u>	<u>1.000</u>	<u>1.000</u>	<u>1.000</u>	<u>571</u>
2.	<u>11.00</u>		<u>22</u>	<u>1.000</u>	<u>1.000</u>	<u>1.000</u>	<u>277</u>
3.	<u>11.00</u>		<u>17</u>	<u>1.000</u>	<u>1.000</u>	<u>1.000</u>	<u>231</u>
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c <u>1041</u>	P _c ² <u>1083681</u>		
NO.	P _t ²	P _w ²	P _c ² - P _w ²
1	<u>289</u>	<u>131</u>	<u>190.4</u>
2			
3			
4			
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{1.017}$

ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{232}$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.009}$

Absolute Open Flow <u>23</u> Mcfd @ 15.025	Angle of Slope θ _____	Slope, n <u>.75</u>
Remarks: <u>Bob Ivy</u>		
Approved By Commission:	Conducted By:	Calculated By:
		Checked By: