NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 10-9-78	
Company: Getty Oil Company	Connection: Not Connected			
Pool: Bloomfield	Formation: Chacra			Unit
Completion Date: 9-29-78	Total Depth: 3100	Plug Back TD: 3053	Elevation: 5573	Farm or Lease Name: E.M.Hartman
Csg. Size: 4.500 / Wt.: 9.500 / d: 4.090 / Set At: 3100		Perforations: From 2952 To 2964		Well No.: 1
Tbg. Size: 1.900 / Wt.: 2.90 / d: 1.610 / Set At: 2954		Perforations: From Open To Ended		Unit: F / Sec.: 13 / Twp.: 29N / Rge.: 11W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single Gas		Packer Set At: -		County: San Jaun
Producing Thru: Tubing	Reservoir Temp. °F: @	Mean Annual Temp. °F	Baro. Press. – P_a: 12.0	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2954	2954	.660				2.000		

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					1057		1057		239 Hr SI
1.	2.000 X .750				123	60	485		1st Hr
2.	2.000 X .750				105	60	410		2nd Hr
3.	2.000 X .750				87	60	377		3rd Hr
4.									
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.00		135	1.000	1.231	1.013	1852
2.	11.00		117	1.000	1.231	1.011	1602
3.	11.00		99	1.000	1.231	1.009	1352
4.							
5.							

NO.	P_r	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1069 P_c^2 1142761

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	9801	389	151321	991440
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1526$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1122$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1,504$

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DIST. 3

Absolute Open Flow 1,504 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .75

Remarks: _____

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	PAUL D.BERHOST	PAUL D.BERHOST	R.P.HERGENRETER