.S.G.S (3), NMOCC (5),
iv. Files, Cen. Rec,
. Archer, D&M,
PNG

NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 9-25-80	
Company: MESA PET. CO	Connection:				
Pool: BASIN DAKOTA	Formation: DAKOTA			Unit: P	
Completion Date: 9-25-80	Total Depth: 6380.	Plug Back TD: 6294.	Elevation: 5670.	Farm or Lease Name: FEDERAL	
Csg. Size: 4.500 / Wt.: 10.5 / d: 4.052 / Set At: 6306.		Perforations: From 6243. To 6304.		Well No.: 9E	
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995 / Set At: 6141.		Perforations: From Ø. To Ø.		Unit: Sec. Twp. Rge.: 9-29N-12W	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: FLOWING		Packer Set At: Ø.		County: SAN JUAN	
Producing Thru: TUBING	Reservoir Temp. °F: 154.@ 6243.	Mean Annual Temp. °F: 60.Ø	Baro. Press. – P_a: 13.2	State: NEW MEXICO	
L: 6243. / H: 6243.	Gg: Ø.673	% CO_2: Ø.	% N_2: Ø.	% H_2S: Ø.	Prover: Ø. / Meter Run: Ø. / Taps:

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							1100.	70.			168.Ø
1.	2.00	X	Ø.750	80.	Ø.	78.	80.	78.	Ø.	Ø.	3.Ø
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.22	Ø.	93.2	Ø.9831	1.2190	1.0089	1265.
2.							
3.							
4.							
5.							

NO.	P_r	Temp. °R	T_r	Z
1.	Ø.14	538.	1.41	Ø.982
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: Ø. Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Ø. Deg.
Specific Gravity Separator Gas: Ø.673 / XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX / Ø.673
Critical Pressure: 669. P.S.I.A. / 669. P.S.I.A.
Critical Temperature: 381. R / 381. R

P_c 1110.6 P_c^2 1233.

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	9.	214.	46.	1187.
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0387$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right] = 1.0789$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1301.$

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OCT 6 1980
OIL CON. COM.
DIST. 3

Absolute Open Flow: 1301. Mcfd @ 15.025 | Angle of Slope θ: 53.1 | Slope, n: Ø.750

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	J. Piece	Garrett Comp. AOF Program	JC Young