

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special			Test Date 4-14-81	
Company SUPRON ENERGY CORPORATION			Connection Southern Union Gathering Company	
Pool Wildcat			Formation Chacra	
Completion Date 4-2-81		Total Depth 3040	Plug Back TD 3009	Elevation 5607
Seq. Size 2.875	Wt. 6.50	d 2.441	Set At 3040	Perforations From 2848 To 2959
Tag. Size No Tubing	Wt.	d	Set At	Perforations From To
Type Well - Single - Blindhead - G.C. or C.O. Multiple Single				Form or Lease Name Zachry
Producing Thru Casing		Reservoir Temp. °F #	Annual Temp. °F	Baro. Press. - P _a 12
L 2838	H	G _o 0.650	% N ₂	% H ₂ S
Prover		Meter Run	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _v	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	2"		3/4"						1099		7 days
1.									184	63°	3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Flow Q, Mhd
1	12.3650		196	0.9971	0.9608	1.019	2366
2.							
3.							
4.							
5.							

NO.	P _i	Temp. °R	T _i	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbon	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1										
2.										
3.										
4.										
5.										

NO.	P _i ²	P _w ²	1/P _w ²	P _i ² - P _w ²
1	1111	1,234,321		60,150
2.				
3.				
4.				
5.				

(1) $\frac{P_c^2}{P_i^2 - P_w^2} = 1.0512$

AOG = Q $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 2456$

(2) $\left[\frac{P_i^2}{P_i^2 - P_w^2} \right]^n = 1.0381$

Absolute Open Flow	2456	Ucid # 15.025	Angle of Slope	0.75
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Approved by Division	Conducted By	Calculated By Kenneth R. Roddis	Checked By
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