

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 4-6-81																									
Company SUPRON ENERGY CORPORATION				Connection Southern Union Gathering Company																									
Pool Bloomfield				Formation Chacara																									
Completion Date 3-18-81		Total Depth 3050		Plug Back TD 3017																									
Elevation 5733		Form or Lease Name Congress		Well No. 10																									
Coq. Size 2.875	Wt. 6.50	d 2.441	Set At 3048	Perforations From 2827 To 2953																									
Trq. Size NO TUBING	Wt.	d	Set At	Perforations From To																									
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single				Packer Set At																									
Producing Thru Casing		Reservoir Temp. °F #		Baro. Press. - P _a 12																									
L 2817		H 0.650		County San Juan																									
Cg		% N ₂		% H ₂ S																									
Prover		Meter Run		Tops																									
FLOW DATA				TUBING DATA																									
CASING DATA				Duration of Flow																									
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Temp. °F																								
1	2"		3/4"																										
2																													
3																													
4																													
5																													
RATE OF FLOW CALCULATIONS																													
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g																								
1	12.3650		143	0.9962	0.9608																								
2																													
3																													
4																													
5																													
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio																								
1																													
2																													
3																													
4																													
5																													
A.P.I. Gravity of Liquid Hydrocarbons																													
Specific Gravity Separator Gas																													
Specific Gravity Flowing Fluid																													
Critical Pressure P.S.I.A.																													
Critical Temperature R																													
Mcf/bbl. Deg.																													
XXXXXX																													
P.S.I.A. R																													
P.S.I.A. R																													
$(1) \frac{P_c^2}{P_t^2 - P_w^2} = 1.0365$ $(2) \left[\frac{P_c^2}{P_t^2 - P_w^2} \right]^n = 1.0272$																													
$AOG = Q \left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 1763$																													
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td>NO.</td> <td>P_t²</td> <td>P_w²</td> <td>P_t² - P_w²</td> </tr> <tr> <td>1</td> <td></td> <td></td> <td>31,791</td> </tr> <tr> <td>2</td> <td></td> <td></td> <td></td> </tr> <tr> <td>3</td> <td></td> <td></td> <td></td> </tr> <tr> <td>4</td> <td></td> <td></td> <td></td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> </tr> </table>						NO.	P _t ²	P _w ²	P _t ² - P _w ²	1			31,791	2				3				4				5			
NO.	P _t ²	P _w ²	P _t ² - P _w ²																										
1			31,791																										
2																													
3																													
4																													
5																													
Absolute Open Flow 1763 Mcd # 15.025 Angle of Slope # Slope, n .75																													
Remarks																													
Approved by Division		Conducted By Cliff Gates		Calculated By John Rector																									
Checked By																													