

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

LIVED
DEC 30 1981
OIL CON. COM.
DIST 3

Type Test ☒ Initial ☐ Annual ☒ Special				Test Date 12-18-81	
Company Amoco Production Company				Connection Amoco Gas Company	
Pool Basin				Formation Dakota	
Completion Date 11-25-81		Total Depth 6405		Plug Back TD 6364	
				Elevation 5694 GL	
Farm or Lease Name Gallegos Canyon Unit					
Csg. Size 4.500	Wt. 10.5	d 4.052	Set At 6405	Perforations: From 6158 To 6288	
Well No. 134E					
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 6284	Perforations: From open To ended	
Unit Sec. Twp. Rge. I 17 29N 12W					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At None	
Producing Thru Tubing				County San Juan	
Reservoir Temp. °F ρ		Mean Annual Temp. °F ρ		Baro. Press. - P _a State New Mexico	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S
Prover		Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI	9 Days						1156		1156	
1.	2.375		.750				65		343	3 hrs
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		77	1.000	.9258	1.009	889
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1168	P _c ² 1364224		
NO.	P _w	P _w ²	P _c ² - P _w ²
1	355	126025	1238199
2			
3			
4			
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.1018$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0754$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 956$$

Absolute Open Flow	956	Mcf/d @ 15.025	Angle of Slope θ	Slope, n .75
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Remarks:

Approved By Commission	Conducted By J. J. Barnett	Calculated By J. J. Barnett	Checked By
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