

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 9/3/82					
Company PETROLEUM CORP. OF TEXAS				Connection None						
Pool Aztec Fruitland				Formation Fruitland				Unit		
Completion Date 8/25/82		Total Depth 1995'		Plug Back TD 1831'		Elevation 5558'G.L.		Farm or Lease Name Bunce		
Csg. Size 4.500	Wt. 10.50	d 4.000	Set At 1995'	Perforations: From 1639' To 1659'			Well No. 3			
Thq. Size NONE	Wt. --	d --	Set At --	Perforations: From -- To --			Unit A	Sec. 19	Twp. 29N	Rge. 10W
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single - Gas					Packer Set At		County San Juan			
Producing Thru Casing		Reservoir Temp. °F 102 @ 1995		Mean Annual Temp. °F 60°		Baro. Press. - P _a 12.0		State New Mexico		
L 1639	H	Gg .60	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps		

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							None		565		7 days
1.	3/4 THC						None		224		3 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		238	1.000	1.000	1.000	2942
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 577	P _c ² 332,929			
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	55,696	238	56,513	276,416
2				
3				
4				
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.204$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1709$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3444$$

Absolute Open Flow	3444		Mcf/d @ 15.025	Angle of Slope θ	Slope, n	0.85
Remarks:						

Approved By Commission:	Conducted By: Bill Matthews	Calculated By: Dewayne Blancett	Checked By:
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