OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL 12-18-85

Type Test: [X] Initial [ ] Annual [X] Special				Test Date: 12-26-85	
Company: Amoco Production Co.			Connection: Amoco Gas Company		
Pool: Basin			Formation: Dakota		Unit
Completion Date: 12-10-85	Total Depth: 6200'		Plug Back TD: 6155'	Elevation: 5520' GR	Farm or Lease Name: Gallegos Canyon Unit
Csg. Size: 7.000 / Wt.: 23 / d: 6.366 / Set At: 6200			Perforations: From 5944' To 6066'		Well No.: 109E
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995 / Set At: 6069'			Perforations: From open To ended		Unit: E / Sec.: 18 / Twp.: 29 / Rge.: 12
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: None		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	8 days					1162		1703		
1.	2.375	.750				214		770		3 hours
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		226	1.000	.9258	1.027	2657
2.							
3.							
4.							
5.							

NO.	P_r	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

JAN 22 1986
OIL CON. DIV.
DIST. 3

P_c 1715 P_c^2 2941225

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		782	611524	2329701
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2625$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1910$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3165$

Absolute Open Flow _____ Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .75

Remarks: Did not flare, lite H_2O, lite condensate

Approved By Division	Conducted By: Joe Elledge	Calculated By: J.J. Barnett	Checked By: