1-14xas mat's
1-Bill Parish 1-D NEW MEXICO OIL CONSERVATION COMMISSION
1-Tidewater, Durango
2-Tidewater, Midland
1-N.W. Prod. 1-F

COMPANY\_

Form **¢-122** 

	l-Lion			MUL'	ri-poin	T BA	CK PRES	sure tes	T FOR GAS	S WELLS		Revis	ed 12-1-55	
Poo	1 Undes	igna	ted	<del></del>	_Format	ion_	Me	saverde		_County	San .	Juan		
Ini	tialXAnnu			alSpecial				ial		_Date of	Te <b>st</b>	st10/10/61		
Com	pany South	west	Prod	ucti	on Co.	•L	ease	Paul	Palmer	Wel	1 No	1_		
	Unit L Sec. 26 Twp. 30 Rge. 12 Purchaser El Paso Natural Gas Co.													
Casing       46       Wt.       10.50 I.D.       4.040 Set at       3472 Perf.       Open       To Hole         Tubing       1½       Wt.       2.76 I.D.       1.610 Set at       3474 Perf.       —       To 3474														
	Gas Pay: From 3473 To 3509 L 3474 xG .67 -GL 2327.5 Bar.Press. 12.0													
Proc	Producing Thru: Casing Tubing X Type Well Single Gas  Single-Bradenhead-G. G. or G.O. Dual  Date of Completion: 9/26/61 Packer Reservoir Temp.													
Date	e of Complet	ion:_	9/26/	61	Pa	cker			Reservo	oir Temp			***	
							OBSERV	ED DATA						
Tested Through (Choke) (Netsaxxx								:	Туре Тарз					
Flow Data (Prover) (Choke) Pr					,a			Tubing Data		Casing Data				
No.	(Prover) (Line)	(Ch	oke) <b>Rikeri</b> x	Pres	ss. Di	ff	1		i				Duration of Flow	
İ	Size		Size				°F•		°F.	I .			Hr.	
SI l.		3/4		300		-	<u> </u>	1342 300		1342 862			days hr.	
2.						-	- 07	300		- 002		<del>                                     </del>	111.	
<b>3.</b> ]														
4. 5.		<del> </del>									ļ	<u> </u>		
<u> </u>		L				L		7177 A M T ON	<u> </u>		l	<b>L</b>		
	Coeffici	ent.	1		Pressu	re Fi	Flow CALC	CULATION:	S Gravitv	Compre	55.	Rate of Flow		
No.	7			Fressure			Factor		Factor	Factor		Q-MCFPD		
	(24 <b>-</b> Hou	r)   $\sqrt{h_{W}^{r}}$		f	f psia		F	ε	$^{\mathtt{F}}_{\mathbf{g}}$	Fpv		@ 15.025 psia		
1.	12.3650				312		.991	<u> </u>	.9463	1.03	3	3	.739	
2.														
3.			<del> </del>		<del></del>	-+-							······································	
1. 2. 3. 4.						-				<del></del>	+		<del></del>	
						PRES	SSURE CA	ALCU ATI	ONS					
as I	iquid Hydro	carboi	n Ratio	<b>)</b>		(	cf/bbl.		Speci	fic Gravit	t.v. Sena	ırat.or	Gas	
	ty of Liqui		rocarbo	ns			deg.		Specific Gravity Separator GasSpecific Gravity Flowing Fluid					
'с			(1	е <sup>-s</sup>			<del> </del>		Pc	1354	_P <sup>2</sup>	1833	.3	
	·	<del> </del>			<del></del>				Pw	874	Pw2_	763	.8	
No.	P <sub>w</sub>	$P_{\mathbf{t}}^2 \mid F_{\mathbf{c}}$		Q	(F <sub>c</sub> C	(2) <sup>2</sup>	(F,	$\frac{Q}{e^{-s}}$	$P_w^2$	$P_c^2 - P_w^2$	Ca	1.	P <sub>ur</sub>	
+	Pt (psia)						(1-	-e-s)	••		F	W	P <sub>w</sub> P <sub>c</sub>	
1. 2. 3. 4. 5.					+		<del>-  </del>		763.8	1069.5	<del> </del>		.654	
3.														
4.											-			
5.					1		_i		<del></del>		<u> </u>			
	lute Potent		5.6				MCFPD;	n	75					
COMP	ANY South	west	Produ	eti Bi-	on Con	pan	Y Tanta-	, N.M.			<del></del>			
	ESS 207 P								ngineer				<del></del>	
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REMARKS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (Pw). MCF/da. @ 15.025 psia and 60° F.
- $P_c$ I 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- $F_g$ : Gravity correction factor.
- $F_t$  Flowing temperature correction factor.
- $F_{nv}$  Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\mathbf{w}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{w}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .