NEW MEXICO OIL CONSERVATION COMMISSION

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	1-File										Form C-1 Revised 12-1-
_								EST FOR GA			
iti	al		Annt	ual		Spec	ial	· 	Date of	Test_7	/19/56
											16-15
it	5-1/2	_Sec	15Tw	νρ Ξ /	Re	e	Pur	rchaser			· · · · · · · · · · · · · · · · · · ·
sin	g 7-5/8	_Wt		.D	Se	t at 355	6 1	Perf5260	<u>. </u>	_To5	788
oin	g 2-3/8	<u></u> Wt	I	.D	Se	t at 574	7I	Perf		_To	
s P	ay: Fro	m 52 60	To	5768	L	x	G			Bar.Pre	85. 10 pela
odu	cing Thr	u: (asing_		Tu	bing	I	Type Weingle-Brade	ell <u>Sins</u>	വര	_
:e	of Compl	etion:	7/11/	56	Packe	r	St	ingle-Brade Reservo	enhead-G. oir Temp.	G. or (3.0. Dual
	-,						ED DATA		•		
ste	d Throug	h (🗪		Choke)	(Madager)			·	Tune Tar	ne	Li T
			Flow D		755557	State T		ng Data			Ţ
T	(Prover) (0	hoke)	Press	Diff.	Temp.		Temp.	Casing I		
	(Line) Size	1 -	ifice) Size	psig	h _w	o _F .	psig	o _F .	psig	o _F .	of Flow Hr.
		3/		240		79	1045 240	79	1045		0.75
F			<u> </u>				#**V		92		3 Brs.
\vdash										 	
,						FLOW CAL					· · · · · · · · · · · · · · · · · · ·
Coefficient		Pr		ressure	Flow 'Fac	- 1	Gravity Factor	Compress.		Rate of Flow Q-MCFPD	
	(24-H	our)	√ h _w	$p_{\mathbf{f}}$	psia	F.		Fg	Fpv		@ 15.025 psia
7	.1605			8	52	.9822		1.612	1.017	·	3607
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			· · · · · · · · · · · · · · · · · · ·		ממ	ESSURE C	A COTTE A TE	TONG		L	
							MTOO.WI		,		
	quid Hydi , of Liqu					cf/bbl. deg.					rator Gas ving Fluid
			(1-e ⁻⁵				Pc_1	05A	P _c 11	10.9
I	w		<u>, T</u>					6 44	7 -		
Ì	" Pt (psia)		$P_{\mathbf{t}}^2 \mid \mathbf{F}$	c ^Q	$(F_cQ)^2$	(F	cQ) ² -e ^{-s})	P_{W}^{2}	$P_c^2 - P_w^2$	Ca	$\frac{P_{\mathbf{w}}}{P_{\mathbf{c}}}$
	o (POIG							414.7	696-2		1.69
-		A Vigor									
											
<u> </u>					· · · · · · · · · · · · · · · · · · ·				L		
ioli (PAN	ite Poter IY Pacu	ntial:			er Gerre		n <u>.75</u>	= 1.4226			
RES	SS 4051	W. Br	osdvav.	Farmi	ngton, N	ew <u>Mexi</u> c	0				
	and TIT	ut Co	K. WAG	الله والله	District Control						
PAN											

			Flow D	404			TWDTH	g Data	Casing I	<i>j</i> ata	
٥.	(Prover) (Line)	(Ori	oke) fice)	Press		, -	Press	· Temp.	Press.	Temp.	Duration of Flow
١	Size	S	ize	psig	h _w	°F.	psig	°F.	psig	[⊃] F•	Hr.
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Т	Coefficie	ent		Pi	ressure	FLOW CAL Flow		NS_ Gravity	Compre	ss.	Rate of Flow
•						Fac		Factor	Facto		Q-MCFPD
	(24-Hou	r)	l√ h _w	$p_{\mathbf{f}}$	psia	F	t	${ t F}_{ t g}$	Fpv		@ 15.025 psia
1	14.1605			2	52	.9822		1.012	1.017		3607
Т											
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4		-									
/i	iquid Hydrod ty of Liquid	carbor 1 Hydi	cocarb	o ons l-e ^{-s} }_		cf/bbl.deg.	rioo.wi	Speci	fic Gravi	ty Sepa ty Flov PC 11	arator Gas wing Fluid 19.9
vi ¹	ty of Liquid	l Hydr	rocarb	ons l-e ^{-s}		cf/bbl.deg.		Speci Speci Pc_1	fic Gravi	ty Flov P _C 11	wing Fluid
vi	ty of Liquid	earbor d Hydr	rocarb	ons		cf/bbl.deg.	c ^Q) ² -e ^{-s})	Speci Speci P _c _1	fic Gravi	ty Flov P ² 11	al. Pw Pc
vi	ty of Liquid	l Hydr	rocarb	ons l-e ^{-s}		cf/bbl.deg.	c ^Q) ² -e ^{-s})	Speci Speci Pc_1	fic Gravi	ty Flov P ² 11	uing Fluid
vii	P _w Pt (psia)	l Hydr	rocarb	ons l-e ^{-s}		cf/bbl.deg.	c ^Q) ² -e ^{-s})	Speci Speci P _c _1	fic Gravi	ty Flov P ² 11	il. Pw Pc
vii	P _w Pt (psia)	l Hydr	rocarb	ons l-e ^{-s}		cf/bbl.deg.	c ^Q) ² -e ^{-s})	Speci Speci P _c _1	fic Gravi	ty Flov P ² 11	al. Pw Pc
vi	P _w Pt (psia)	l Hydr	rocarb	ons l-e ^{-s}		cf/bbl.deg.	c ^Q) ² -e ^{-s})	Speci Speci P _c _1	fic Gravi	ty Flov P ² 11	lo. Pw Pc
vii	Pw Pt (psia)	P _t	F F	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	cQ) ² -e-s)	Speci Speci P _c _1	fic Gravi	ty Flov P ² 11	lo. Pw Pc
vii • • soi	Pw Pt (psia)	Pt	F. F.	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	cQ) ² -e-s)	Speci Speci Pc_1 Pw2	fic Gravi	ty Flov P ² 11	lo. Pw Pc
viii • • soi	Pw Pt (psia)	Pt land	F. S.13	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	cQ) ² -e-s)	Speci Speci Pc_1 Pw2	fic Gravi	ty Flov P ² 11	lo. Pw Pc
sol MP/DRI	Pw Pt (psia)	Pt land	F. S.13	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	cQ) ² -e-s)	Speci Speci Pc_1 Pw2	fic Gravi	ty Flov P ² 11	lo. Pw Pc
sol MPA DRI	Pw Pt (psia) lute Potent: ANY PACE 16 ESS 405 W T and TITLE	Pt land	F. S.13	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	n_75 s	Speci Speci Pc_1 Pw2	fic Gravi	ty Flov P ² 11	lo. Pw Pc
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sol MPA	Pw Pt (psia) lute Potent ANY ESS 4054 W T and TITLE ESSED	Pt land	F. S.13	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	n_75 s	Speci Speci Pc_1 Pw2	fic Gravi	ty Flov P ² 11	lo. Pw Pc
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sol MPA DRI	Pw Pt (psia) lute Potent ANY ESS 4054 W T and TITLE ESSED	Pt land	F. S.13	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	n_75 s	Speci Speci Pc_1 Pw2	fic Gravi	Ca I	ving Fluid 19.9 Al. Pw Pc 1.69
sol MPA DRI	Pw Pt (psia) lute Potent ANY ESS 4054 W T and TITLE ESSED	Pt land	F. S.13	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	n_75 s	Speci Speci Pc_1 Pw2	fic Gravi	Ca I	PW PC 1.60
sol MP/DRI	Pw Pt (psia) lute Potent ANY ESS 4054 W T and TITLE ESSED	Pt land	F. S.13	ons l-e ^{-s})	(F _c Q) ²	cf/bbl.deg. (F) (1) MCFPD;	n_75 s	Speci Speci Pc_1 Pw2	fic Gravi	Ca I	ving Fluid 19.9 Al. Pw Pc 1.69

INSTRUCTIONS

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This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (Pw). MCF/da. @ 15.025 psia and 600 F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia

- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- P_{f} Meter pressure, psia.
- $h_{\mbox{W}}\mbox{{\fontfame}}$ Differential meter pressure, inches water.

- Fg Gravity correction factor.
- F_t Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.

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