

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 9-11-80	
Company SUPRCN ENERGY CORPORATION				Connection Southern Union Gathering Company			
Pool Basin				Formation Dakota		Unit	
Completion Date 8-23-80		Total Depth 8160		Plug Back TD 8145		Elevation 6553	
Form or Lease Name Nordhaus		Well No. 2-A		Perforations: From 7894 To 7976		Unit Sec. Twp. Rge. C 11 31N 9W	
Perf. Size 7.625 5.500		Wt. 26.40 15.50		Set At 6.969 4.950 3583-8160		Perforations: No Perforations	
Perf. Size 2.0625		Wt. 3.25		Set At 1.750 7840		Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual - Gas - Gas						Factor Set At 7840	
Producing Thru Tubing		Reservoir Temp. °F 6		Mean Annual Temp. °F 12		State San Juan	
L 7830		H		Gg 0.650		% CO ₂ % N ₂ % H ₂ S Prover Meter Run Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2"		3/4"				1769				7 days
1.							56	60°			3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd
1	12.3650		68	1.0000	0.9608	1.000	808
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.L. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _t 1781	P _c ² 3,171,961		
NO.	P _t ²	P _w	P _w ²
1			40,097
2.			
3.			
4.			
5.			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0128$		(2) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0095$	
AOP = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 816$			

Absolute Open Flow 816	Mcf/d @ 15.025	Angle of Slope θ	Slope, n 0.75
Remarks:			

Approved By Commission:	Conducted By: Steve Moore	Calculated By: Kenneth E. Roddy	Checked By:
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