STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 10-27-81	
Company: Southland Royalty Company			Connection: Southern Union Gathering		
Pool: Flora Vista			Formation: Gallup		Unit
Completion Date: 9-30-81	Total Depth: 6930'		Plug Back TD: 6885'	Elevation: 5986' GR	Farm or Lease Name: Holder "A"
Csg. Size: 5.500 / Wt.: 15.5# / d: 4.950 / Set At: 6930'			Perforations: From To		Well No.: 1-E
Tbg. Size: 1.900 / Wt.: 2.76# / d: 1.610 / Set At: 6068'			Perforations: From 5850' To 6098'		Unit: H / Sec.: 6 / Twp.: 30N / Rge.: 12W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Multiple - G.G.			Packer Set At: 6208'		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F:	Mean Annual Temp. °F:	Baro. Press. – P_a: 12.2		State: New Mexico
L	H	Gg: .700	% CO_2	% N_2	% H_2S / Prover / Meter Run / Taps

FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI										
1.	2"	X 3/4"				504		504		
2.						43		251		1 hr
3.						19		261		2 hrs
4.						21		251		3 hrs
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		33.2	1.0000	.9258	1.0000	380
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXXX
Specific Gravity Flowing Fluid _____ XXXXXX
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 516.2 P_c^2 266462.4

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		263.2	69274.2	197188.2
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3513$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.3533$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 476$

NOV 5 1981
OIL CON. COM.
DIST. 3

Absolute Open Flow 476 Mcfd @ 15.025 | Angle of Slope θ _____ | Slope, n .75

Remarks: _____

Approved By Division	Conducted By:	Calculated By:	Checked By:
	Jim Bacon	James Smith	L. O. Van Ryan