3 NMOCD 1 Ladd, DE 1 Terry Jones 1 File

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [XX] Initial [ ] Annual [ ] Special					Test Date: 8-26-82				
Company: Ladd Petroleum Corp.				Connection:					
Pool: Basin Dakota				Formation: Dakota				Unit:	
Completion Date: 8-11-82		Total Depth: 6434		Plug Back TD: 6393'		Elevation: 5803 GL		Farm or Lease Name: Butte	
Csg. Size: 4½"	Wt.: 10.5#	d: 4.052	Set At: 6434'	Perforations: From 6184	To 6316			Well No.: 1E	
Tbg. Size: 1½"	Wt.: 2.9#	d: 1.610	Set At: 6245'	Perforations: From none	To			Unit: M Sec.: 8 Twp.: 30N Rge.: 13W	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: single				Packer Set At: none				County: San Juan	
Producing Thru: tubing	Reservoir Temp. °F: 155 @ 6405		Mean Annual Temp. °F:	Baro. Press. – P_a: 12.2 psia				State: NM	
L	H	Gg: 0.65	% CO_2: -0-	% N_2: -0-	% H_2S: -0-	Prover: --	Meter Run: --	Taps: ---	

FLOW DATA

NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI					1320		1330	--	7 days
1.	9/16" pos. choke	--	--	--	110	65	560	--	3 hrs.
2.									
3.									
4.									
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	6.8979	--	122	0.9952	0.9608	1.011	814
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_t	Z
1				
2.				
3.				
4.				
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1342 P_c^2 1,800,964

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		572	327,184	1,473,780
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.22$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.16$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 946

Absolute Open Flow 946 Mcfd @ 15.025 Angle of Slope θ 53° Slope, n .75

Remarks: Light spray of condensate and water throughout test.

Approved By Division	Conducted By: S. Dugan	Calculated By: J. Roe	Checked By: J. Jacobs