

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL.

Form C-122
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 10/3/84		RECEIVED						
Company Union Texas Petroleum Corp.			Connection Southern Union Gathering Company							
Pool Basin			Formation Dakota							
Completion Date 8/9/84		Total Depth 6512		Plug Back TD 6463						
				Elevation 5695						
Farm Code Name McCord		Unit CON. DIV. DET. 2								
Crg. Size 4.500		Wt. 11.60		d 4.000						
Set At 6512		Perforations: From 6242		To 6408						
Tbg. Size 2.375		Wt. 4.70		d 1.995						
Set At 6399		Perforations: From 6336		To 6342						
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single			Packer Set At -----		County San Juan					
Producing Thru Tubing		Reservoir Temp. °F @		Mean Annual Temp. °F						
				Baro. Press. - P _g 12						
State New Mexico										
L 6329	H	G _g 0.650	% CO ₂	% N ₂	% H ₂ S					
Prover	Meter Run	Taps								
FLOW DATA			TUBING DATA			CASING DATA		Duration of Flow		
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.		Temp. °F	Press. p.s.i.g.
SI	2"		3/4"				1920		2000	
1.							298	85°	696	
2.										
3.										
4.										
5.										
RATE OF FLOW CALCULATIONS										
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd			
1	12.3650		310	0.9768	0.9608	1.025	3687			
2.										
3.										
4.										
5.										
NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.					
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.					
2.					Specific Gravity Separator Gas _____ X X X X X X X X X					
3.					Specific Gravity Flowing Fluid _____ X X X X X					
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.					
5.					Critical Temperature _____ R _____ R					
P _c	2012	P _c ²	4,048,144							
NO.	P _i ²	P _w	I _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1413$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1041$				
1		708	501,264	3,546,880						
2										
3										
4										
5										
AOI = Q						$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4071$				
Absolute Open Flow		4071		Mcf/d @ 15.025		Angle of Slope @		Slope, n 0.75		
Remarks:										
Approved By Commission:			Conducted By: Floyd Woodward			Calculated By: Ken Roddy			Checked By:	