STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION

P O BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 1-13-88	
Company: Union Texas Petroleum Corp	Connection: Sunterra Gas Gathering Co.			
Pool: Blanco	Formation: Mesaverde		Unit	
Completion Date: 12-17-87	Total Depth: 5588	Plug Back TD: 5535	Elevation: 6070' G.L.	Farm or Lease Name: Quinn
Csg. Size: 7.000 / 4.500 — Wt.: 23.0 / 10.5 — d: 6.366 / 4.052 — Set At: 3202 / 2999-5588 — Perforations: From 4865 To 5489				Well No.: 8-A
Tbg. Size: 2.375 — Wt.: 4.7 — d: 1.995 — Set At: 5440 — Perforations: From 5411 To 5417				Unit: J — Sec.: 18 — Twp.: 31N — Rge.: 8W
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: Single - Gas		Packer Set At: -----		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F:	Mean Annual Temp. °F:	Baro. Press. - P_a: 12	State: New Mexico
L	H	Gg: .665	% CO_2	% N_2 — % H_2S — Prover — Meter Run — Taps

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI	2"	3/4"				730		750		7 Days
1.						180		640	61°	3 Hours
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		192	0.9990	0.9498	1.020	2298
2							
3							
4							
5							

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DIST. 3

NO.	P_r	Temp. °R	T_r	Z
1				
2				
3				
4				
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 762 P_c^2 580,644

NO	P_w	P_w^2	$P_c^2 - P_w^2$
1	652	425,104	155,540
2			
3			
4			
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.7331$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.6856$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 6172$

Absolute Open Flow 6172 Mcfd @ 15.025 — Angle of Slope θ _____ — Slope, n 0.75

Remarks: Heavy mist of oil

Approved By Division	Conducted By:	Calculated By:	Checked By:
	Connie Clevenger	John C. Rector	