

W MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☐ Initial ☐ Annual ☒ Special					Test Date 9-1-77																																																																																
Company Aztec Oil & Gas Company				Connection None																																																																																	
Pool Basin				Formation Dakota		Unit																																																																															
Completion Date		Total Depth		Plug Back TD		Elevation																																																																															
Farm or Lease Name Uells Canyon																																																																																					
Csg. Size	Wt.	d	Set At	Perforations: From To		Well No. #1																																																																															
Tbg. Size	Wt.	d	Set At	Perforations: From To		Unit Sec. Twp. Rge. M 21 32 5																																																																															
Type Well - Single - Bradenhead - G.G. or G.O. Multiple					Packer Set At																																																																																
Producing Thru		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a 12.2																																																																															
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover Meter Run Taps																																																																															
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th colspan="4">FLOW DATA</th> <th colspan="2">TUBING DATA</th> <th>CASING DATA</th> <th rowspan="2">Duration of Flow</th> </tr> <tr> <th>NO.</th> <th>Prover Line Size</th> <th>X</th> <th>Orifice Size</th> <th>Press. p.s.i.g.</th> <th>Diff. h_w</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> <th>Press. p.s.i.g.</th> <th>Temp. °F</th> </tr> <tr> <td>1.</td> <td>2"</td> <td>X</td> <td>3/4"</td> <td></td> <td></td> <td></td> <td>384</td> <td></td> <td>143</td> <td></td> <td></td> </tr> <tr> <td>2.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>50#-</td> <td></td> <td>203</td> <td></td> <td>1 hr</td> </tr> <tr> <td>3.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>50#-</td> <td></td> <td>226</td> <td></td> <td>2 hrs</td> </tr> <tr> <td>4.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>61#</td> <td></td> <td>233</td> <td></td> <td>3 hrs</td> </tr> <tr> <td>5.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> </table>							FLOW DATA				TUBING DATA		CASING DATA	Duration of Flow	NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	1.	2"	X	3/4"				384		143			2.							50#-		203		1 hr	3.							50#-		226		2 hrs	4.							61#		233		3 hrs	5.											
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RATE OF FLOW CALCULATIONS																																																																																					
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd																																																																														
1	12.365		73.2	1.0000	.9258	1.0000	838																																																																														
2																																																																																					
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NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ X X X X X X X X X Specific Gravity Flowing Fluid _____ X X X X X Critical Pressure _____ P.S.I.A. _____ P.S.I.A. Critical Temperature _____ R _____ R																																																																																
P _c 396.2 P _c ² 156,974					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.6208$ $\frac{P_c^2}{P_c^2 - P_w^2} = 1.4364$																																																																																
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	AOF = $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1,204$																																																																																
1		245.2	60,123	96,851																																																																																	
2																																																																																					
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Absolute Open Flow 1,204 Mcfd @ 15.025					Angle of Slope θ		Slope, n .75																																																																														
Remarks:																																																																																					
Approved By Commission:		Conducted By: Klee Terry		Calculated By: James Smith		Checked By: <i>[Signature]</i>																																																																															

