MULTI-POINT DACK PRESSURE TEST FOR GAS WELLS

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T-/2/1/1	'			endanes relicer c		ED DATA				
//-7217' 'F- 1911 ested Thro	ich (Dm	over) (Chalea)	(Moton)		23.7		Тита Тап	ve.	
ested Through (Prover) (Choke) (Meter)						·	Type Taps			
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o. (Line Size	e) (Or		psig	h _w	o _F .	psig	°F.	psig	o _F .	of Flow Hr.
I				"		21-8				
•		<u> </u>		-		117		2772		- 3 hours
				I	FLOW CAL	CULATIO	NS			
Coef	Coefficient		Pr	Pressure Flow		Temp.	Gravit.v	Compress.		ate of Flow Q-MCFPD
$(24-\text{Hour}) \sqrt{h_{\text{W}}p_{\text{f}}}$		o _f	psia		t	Fg	F _{pv}		@ 15.025 psia	
12.36	12,3650		129		•992lı		.96	1,011 1,53		1,:38
s Liquid Hy avity of Li		drocarb			cf/bbl. deg.		Speci Speci	fic Gravi fic Gravi	ty Separ ty Flowi P ²	ator Gas ng Fluid <u>650</u>
P _w	a)	$P_{\mathbf{t}}^2 = \mathbf{F}$	_c Q	(F _c Q) ²	(F (1	cQ) ² -e ^{-s})	P _w 2	$P_c^2 - P_w^2$	Cal P _w	P _W P _C
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solute Por	ential:	— 1/ x	0		MCFPD;	n	•75			
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-		7			REM	ARKS		/ 011	CON. CC DIST. 3	J.

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (P_W) . MCF/da. @ 15.025 psia and 60° F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- P_{w} Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- P_f Meter pressure, psia.
- $h_{\mbox{W}}$ Differential meter pressure, inches water.
- F_g : Gravity correction factor.
- F_t Flowing temperature correction factor.
- F_{DV} Supercompressability factor.
- n I Slope of back pressure curve.

Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.

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