MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

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ate	e of Complet	ion:_ 16 _	25-61	Packe:	Set at	odel "D" 6550' ED DATA	Reservo	ir Temp				
e s 1	ed Through	(Prover	(Choke)	(Meter)				Type Tap:	s			
			w Data	Diag	M			Casing Da			Duration	
ю.	(Prover) (Line)				_	•					of Flow	
I	Size	Size	psig	h _w	F.		F.	psig	-F.	<u> </u>	Hr.	
		3/4"			600	1781		913		3 hours		
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	Coeffici	ressure	FLOW CALCULATION Pessure Flow Temp.			Gravity Compress. Rate of Flow Factor Factor Q-MCFPD						
No.	(24-Hour) √h		hwpf	1 . 1		Factor Ft		Fpv			15.025 psi	
	12,3650				75 1.0		Fg Fpv		00		859	
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av	Liquid Hydro ity of Liqui 1,6025	d Hydroc	arbons		cf/bbl.deg		Speci Speci	ific Gravi ific Gravi 955	ty Flo		luid	
۱o.	P _w	Pt ²	F _c Q	(F _c Q) ²	! (1	F _c Q) ² 1-e ^{-s})	P _w 2	$P_c^2 - P_w^2$	1	al.	P _W P _C	
[.	Pt (psia)	5,625	3.095	9.57			7.560	904.465		7	.091	
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4. 5.								 	+	+		
<u>, </u>	olute Potent	ial•	864	1	MCFPD	: n	0.75	· · · · · · · · · · · · · · · · · · ·				
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INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w). MCF/da. @ 15.025 psia and 600 F.
- Pc= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If $P_{\rm W}$ cannot be taken because of manner of completion or condition of well, then $P_{\rm W}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\rm t}$.