MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool		Basin	Dakota	F	ormation	<u> </u>	Dakota		_County_	Sen	Juan	
Init	ial	<u> </u>	Annu	al		Spec	ial		_Date of	Test_	11-26-62	
Compa	any South	ern Un	ion Prod	nation	Co.	Lease	Talia	ferre	We]	ll No	3	
Unit		Sec.	31_Twp	o31	North Rg	e. <u>12 i</u>	Purc	haser So r	thern Un	lon Gar	Company	
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						OBSERV	ED DATA					
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	(Prove	r) (Flow Da	Press. Dif		f. Temp.		Data Temp.	Casing I	Temp.	Duration	
No.		(01	rifice)		h _w	,		o _F ,		ļ	of Flow	
SI							1912		1954		7 days	
1. 2.	2#		3/4	206	<u> </u>	660	206	660	963		3 hours	
<u>3. [</u>										-		
4. 5.									 -	 		
						FLOW CAL	CIT.ATTON	S				
	Coeff	Coefficient		Pr	ressure Flow		Temp.	Gravity			Rate of Flow Q-MCFPD @ 15.025 psia	
No.	(24-Hour)		¬√ hwr	—			tor	Factor F _o	Facto	r		
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4.												
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1. 2.								950.6	291)		-1496	
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COMPA ADDRE						oduction.	Company					
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INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w). MCF/da. @ 15.025 psia and 60° F.
- P_c= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- P_t Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- F_{pv} Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.