

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-65

|                                                                                                                           |            |                         |                                        |                                  |                                                       |
|---------------------------------------------------------------------------------------------------------------------------|------------|-------------------------|----------------------------------------|----------------------------------|-------------------------------------------------------|
| Type Test<br><input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special |            |                         |                                        | Test Date<br>10-20-68            |                                                       |
| Company<br>Aztec Oil and Gas                                                                                              |            |                         | Connection<br>Southern Union Gathering |                                  |                                                       |
| Pool<br>Antec                                                                                                             |            |                         | Formation<br>Pacheco Shale             |                                  | Unit                                                  |
| Completion Date<br>10-16-68                                                                                               |            | Total Depth<br>2434     | Perforation TD<br>2433                 | Elevation<br>5239 Gr             | Farm or Lease Name<br>Thurston                        |
| Cou. Size<br>1 1/2                                                                                                        | Wt.<br>9.6 | d                       | Set At<br>2433                         | Perforation<br>From 2406 To 2430 | Well No.<br>1                                         |
| Tub. Size<br>1 1/2                                                                                                        | Wt.<br>2.0 | d                       | Set At<br>2412                         | Perforation<br>From 2406 To 2430 | Unit    Sec.    Twp.    Rge.<br>E    31    31N    11W |
| Type Well - Single - Pradhead - G.G. or G.O. Multiple<br>single                                                           |            |                         |                                        |                                  | County<br>San Juan                                    |
| Producing Thru<br>tubing                                                                                                  |            | Reservoir Temp. °F<br>8 | Mean Annual Temp. °F                   | Sat. Press. - P <sub>g</sub>     | State<br>New Mexico                                   |
| L                                                                                                                         | H          | G <sub>g</sub>          | % CO <sub>2</sub>                      | N <sub>2</sub>                   | H <sub>2</sub> S    Prover    Meter Run    Taps       |

  

| FLOW DATA |                  |   |              |                 |                      | TUBING DATA |                 | CASING DATA |                 | Duration of Flow |
|-----------|------------------|---|--------------|-----------------|----------------------|-------------|-----------------|-------------|-----------------|------------------|
| NO.       | Prover Line Size | X | Orifice Size | Press. p.s.i.g. | Diff. h <sub>w</sub> | Temp. °F    | Press. p.s.i.g. | Temp. °F    | Press. p.s.i.g. |                  |
| SI        | 2                |   | 3/4          |                 |                      |             | 578             |             | 578             |                  |
| 1.        |                  |   |              |                 |                      |             | 123             |             |                 |                  |
| 2.        |                  |   |              |                 |                      |             |                 |             |                 |                  |
| 3.        |                  |   |              |                 |                      |             |                 |             |                 |                  |
| 4.        |                  |   |              |                 |                      |             |                 |             |                 |                  |
| 5.        |                  |   |              |                 |                      |             |                 |             |                 |                  |

  

| RATE OF FLOW CALCULATIONS |                       |                  |                         |                                  |                               |                                          |                            |
|---------------------------|-----------------------|------------------|-------------------------|----------------------------------|-------------------------------|------------------------------------------|----------------------------|
| NO.                       | Coefficient (24 Hour) | $\sqrt{h_w P_m}$ | Pressure P <sub>m</sub> | Flow Temp. Factor F <sub>t</sub> | Gravity Factor F <sub>g</sub> | Super. Compress. Factor, F <sub>pv</sub> | Rate of Flow Q, bbl. / day |
| 1                         | 12.355                |                  | 57                      | 1.000                            | .9258                         | 1.009                                    |                            |
| 2                         |                       |                  |                         |                                  |                               |                                          |                            |
| 3                         |                       |                  |                         |                                  |                               |                                          |                            |
| 4                         |                       |                  |                         |                                  |                               |                                          |                            |
| 5                         |                       |                  |                         |                                  |                               |                                          |                            |

  

| NO. | P <sub>r</sub> | Temp. °R | T <sub>r</sub> | Z | Gas-Liquid Hydrocarbon Ratio | A.P.L. Gravity of Liquid Hydrocarbons | Specific Gravity Separator Gas | Spec. Gr. Gravity Flowing Fluid | P.S.I.A. | P.S.I.A. |
|-----|----------------|----------|----------------|---|------------------------------|---------------------------------------|--------------------------------|---------------------------------|----------|----------|
| 1   |                |          |                |   |                              |                                       |                                |                                 |          |          |
| 2   |                |          |                |   |                              |                                       |                                |                                 |          |          |
| 3   |                |          |                |   |                              |                                       |                                |                                 |          |          |
| 4   |                |          |                |   |                              |                                       |                                |                                 |          |          |
| 5   |                |          |                |   |                              |                                       |                                |                                 |          |          |

  

|                       |                       |                       |                       |                       |                       |                       |                       |                       |                        |                        |                        |                        |                        |                        |                        |                        |                       |                       |                       |                       |                       |                       |                       |                       |                       |                      |                     |                     |                     |
|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|----------------------|---------------------|---------------------|---------------------|
| P <sub>1</sub> = 530  | P <sub>2</sub> = 300  | P <sub>3</sub> = 260  | P <sub>4</sub> = 240  | P <sub>5</sub> = 230  | P <sub>6</sub> = 220  | P <sub>7</sub> = 210  | P <sub>8</sub> = 200  | P <sub>9</sub> = 190  | P <sub>10</sub> = 180  | P <sub>11</sub> = 170  | P <sub>12</sub> = 160  | P <sub>13</sub> = 150  | P <sub>14</sub> = 140  | P <sub>15</sub> = 130  | P <sub>16</sub> = 120  | P <sub>17</sub> = 110  | P <sub>18</sub> = 100 | P <sub>19</sub> = 90  | P <sub>20</sub> = 80  | P <sub>21</sub> = 70  | P <sub>22</sub> = 60  | P <sub>23</sub> = 50  | P <sub>24</sub> = 40  | P <sub>25</sub> = 30  | P <sub>26</sub> = 20  | P <sub>27</sub> = 10 | P <sub>28</sub> = 0 |                     |                     |
| Q <sub>1</sub> = 3308 | Q <sub>2</sub> = 2600 | Q <sub>3</sub> = 2400 | Q <sub>4</sub> = 2300 | Q <sub>5</sub> = 2200 | Q <sub>6</sub> = 2100 | Q <sub>7</sub> = 2000 | Q <sub>8</sub> = 1900 | Q <sub>9</sub> = 1800 | Q <sub>10</sub> = 1700 | Q <sub>11</sub> = 1600 | Q <sub>12</sub> = 1500 | Q <sub>13</sub> = 1400 | Q <sub>14</sub> = 1300 | Q <sub>15</sub> = 1200 | Q <sub>16</sub> = 1100 | Q <sub>17</sub> = 1000 | Q <sub>18</sub> = 900 | Q <sub>19</sub> = 800 | Q <sub>20</sub> = 700 | Q <sub>21</sub> = 600 | Q <sub>22</sub> = 500 | Q <sub>23</sub> = 400 | Q <sub>24</sub> = 300 | Q <sub>25</sub> = 200 | Q <sub>26</sub> = 100 | Q <sub>27</sub> = 0  | Q <sub>28</sub> = 0 | Q <sub>29</sub> = 0 | Q <sub>30</sub> = 0 |

  

|                    |     |             |                  |                |
|--------------------|-----|-------------|------------------|----------------|
| Absolute Open Flow | 664 | Yield 15.25 | Angle of Slope 0 | Slope, n = .85 |
|--------------------|-----|-------------|------------------|----------------|

  

|                         |               |                |             |
|-------------------------|---------------|----------------|-------------|
| Remarks:                |               |                |             |
| Approved By Commission: | Conducted By: | Calculated By: | Checked By: |