

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special				Test Date: 6-22-70	
Company: <u>Aztec Oil & Gas Company</u>			Connection: <u>Southern Union Gathering</u>		
Pool: <u>Undesignated</u>			Formation: <u>Pictured Cliffs</u>		Unit:
Completion Date: <u>6-15-70</u>		Total Depth: <u>2835'</u>	Plug Back TD: <u>2835'</u>	Elevation: <u>6219 Gr</u>	Farm or Lease Name: <u>Patterson</u>
Csg. Size: <u>4 1/2"</u>	Wt.: <u>4.9</u>	d: <u>2830'</u>	Set At: <u>2830'</u>	Perforations: From <u>2738</u> To <u>2786</u>	Well No.: <u>#3</u>
Thq. Size: <u>1.315</u>	Wt.: <u>1.7</u>	d: <u>2737</u>	Set At: <u>2737</u>	Perforations: From <u>----</u> To <u>----</u>	Unit: <u>N</u> Sec. <u>2</u> Twp. <u>31</u> R. <u>12</u>
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: <u>Single</u>				Packer Set At: <u>----</u>	
Producing Thru: <u>Casing</u>		Reservoir Temp. °F: <u>@</u>	Mean Annual Temp. °F: <u>@</u>	Baro. Press. - P _a : <u>----</u>	County: <u>San Juan</u>
L: <u>----</u> H: <u>----</u> G _g : <u>----</u>		% CO ₂ : <u>----</u>	% N ₂ : <u>----</u>	% H ₂ S: <u>----</u>	Prover: <u>----</u> Meter Run: <u>----</u> Taps: <u>----</u>

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI									869	
1.	2"		3/4						50	
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		50	1.0000	.9258	1.0000	572
2.							
3.							
4.							
5.							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c <u>881</u>	P _c ² <u>776,161</u>				
NO.	P _w ²	P _w	P _w ²	P _c ² - P _w ²	
1		62	3,844	772,317	
2					
3					
4					
5					

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.0049}{1.0049} = 1.0049$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.0041}{1.0041} = 1.0041$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 574$

Absolute Open Flow <u>574</u> Mcfd @ 15.025	Angle of Slope Θ _____
Remarks: _____	
Approved By Commission: _____	Conducted By: _____
Calculated By: <u>[Signature]</u>	Checked By: _____

