

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 8-25-73	
Company Aztec Oil & Gas Company				Connection		
Pool Basin				Formation Dakota		Unit
Completion Date 8-13-73		Total Depth 8707'		Plug Back TD 8707'		Elevation 7048 GR
Farm or Lease Name Reese Mesa		Well No. #4				
Casing Size 4 1/2"	Casing Weight 20# & 23#	Set At 6529' 8707'	Perforations: From 8510 To 8662		Unit Sec. Twp. Rge. K 11 32N 8W	
Tubing Size 2 3/8"	Tubing Weight 4.70# 2.90#	Set At 8500' 6191'	Perforations: From To		County San Juan	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Multiple				Packer Set At 8500'		State New Mexico
Producing Thru Tubing		Reservoir Temp. °F @	Mean Annual Temp. °F		Baro. Press. - P _a	
L	H	G _g	% CO ₂	% N ₂	% H ₂ S	Prover
Meter Run		Taps				

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							2567				78
1.	2"		3/4				67				3 hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12,365		67	1.0000	.9258	1.0000	767
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

$P_c = 2,567$ $P_c^2 = 6,589,489$					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.0034$	$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0025$
NO.	P _t	P _w	P _w ²	P _c ² - P _w ²		
1						
2						
3						
4						
5						

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 769$

$\frac{P_c^2}{P_c^2 - P_w^2} = 1.0034$

Absolute Open Flow	769	Mcf/d @ 15.025	Angle of Slope θ	Slope, n
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Remarks:

Approved By Commission:	Conducted By:	Calculated By: 	Checked By:
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