

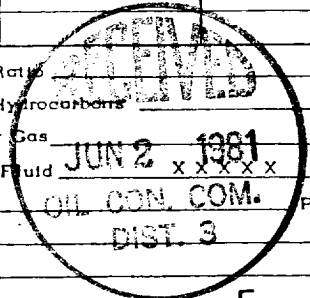
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5-20-81	
Company Southland Royalty Company				Connection Northwest Pipeline Corporation		
Pool Undesignated				Formation Pictured Cliffs		Unit
Completion Date 5-10-81		Total Depth 3720'		Plug Back TD 3689'		Elevation 6667' GR
Farm or Lease Name Reese Mesa		Well No. 9				
Csq. Size 4.500	Wt. 10.5#	d 4.052	Set At 3720'	Perforations: From 3498' To 3620'		Unit Sec. Twp. Rge. D 13 32N 8W
Tng. Size 1.900	Wt. 2.9#	d 1.610	Set At 3608'	Perforations: From To		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single - G.G.				Packer Set At -----		County San Juan
Producing Thru Tubing		Reservoir Temp. °F 8		Mean Annual Temp. °F		State New Mexico
Baro. Press. - P _a 12.2						
L	H	G _g .700	% CO ₂	% N ₂	% H ₂ S	Prover
Meter Run		Taps				

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							589		1546		
1.	2"	X	3/4"				190		895		1 hr
2.							131		750		2 hrs
3.							106		673		3 hrs
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		118.2	1.0000	.9258	1.0000	1353
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas	XXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXXX
4.					Critical Pressure	P.S.I.A.
5.					Critical Temperature	R



P _c 1558.2 P _c ² 2427987.2				
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1		685.2	469499.0	1958488.2
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2397$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1624}{*}$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.2004$

Absolute Open Flow	1624	Mcf/d @ 15.025	Angle of Slope θ	Slope, n .85
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Remarks:

Approved By Division	Conducted By: Don Thompson	Calculated By: James Smith	Checked By: L.O. Van Ryan
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