NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 3-6-82	
Company: Union Texas Petroleum Corporation	Connection: Gas Company of New Mexico			
Pool: Basin	Formation: Dakota		Unit	
Completion Date: 2-25-82	Total Depth: 7001	Plug Back TD: 6975	Elevation	Farm or Lease Name: Culpepper Martin
Csg. Size: 7.625 / 5.500 — Wt.: 26.4 / 15.5 — d: 6.969 / 4.950 — Set At: 4392 / 4267/6999		Perforations: From 6692 To 6918		Well No.: 3M
Tbg. Size: 2 3/8 — Wt.: 4.7 — d: 1.995 — Set At: 6881		Perforations: From open To ended		Unit: F — Sec.: 7 — Twp.: 31 — Rge.: 12
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: G.G. /Dual		Packer Set At: 4822		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a: 12 psia	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
		.650						

	FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	9 days					2052				
1.	2 "	.750	481			481	60° est.			3 hours
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		493	1.000	.9608	1.051.	6156
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2				
3.				
4.				
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid _____ XXXXXXXX
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

RECEIVED
APR 5 1982
OIL CON. DIV.
DIST. 3

P_c 2064 P_c^2 4260096

NO	P_t	P_w	P_w^2	$P_c^2 - P_w^2$
1		1083	1174334	3085762
2				
3		calculated		
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.38056$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.27362$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 7840$

Absolute Open Flow 7840 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n .75

Remarks: Dry gas with show of oil.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Joe Elledge	Joe Elledge	Mr. Don Wells