

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5/21/84		RECEIVED JUN 15 1984 CON. DIV. DIST. 3		
Company Consolidated Oil & Gas, Inc.				Connection Southern Union					
Pool Basin Dakota				Formation Dakota			Unit		
Completion Date		Total Depth 6800'		Plug Back TD 6754		Elevation 5834' KB		Farm or Lease Name Payne	
Csq. Size 5 1/2	Wt. 17# & 15.5#	d 4.950	Set At 6796'	Perforations: From 6500 To 6601			Well No. 2-E		
Tq. Size 1 1/2	Wt. 2.9#	d 1.610	Set At 6623'	Perforations: From To			Unit Sec. Twp. Age E 35 31 13		
Type Well - Single - Broadhead - G.C. or G.O. Multiple Dual gas						Packer Set At 5992		County San Juan	
Producing Thru Tubing		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a 12.0		State New Mexico	
L	H	G _g .650	% CO ₂	% N ₂	% H ₂ S	Prover 6" choke	Meter Run Nipple	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	15 days						1231		Pkr.		
1.	2 x 3/4						124	60	Pkr.		3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	11.00		136	1.000	1.240	1.013	1879
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1243	P _c ² 1545049	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2163$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1581$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1.		524	274.800	1270249
2.				
3.				
4.				
5.				

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2176$$

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Absolute Open Flow 2176	Mcf/d @ 15.025	Angle of Slope 53.13°	Slope, n 0.75
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Remarks:

Conducted By:
Calculated By:
Checked By: