STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

JUL 20 1984
OIL CON. DIV.
DIST. 3

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 7-3-84		
Company: Consolidated Oil & Gas, Inc.		Connection: Southern Union Gathering Co.			
Pool: Basin Dakota		Formation: Dakota		Unit	
Completion Date: 5-29-84	Total Depth: 6680		Plug Back TD: 6646	Elevation: 5645 GL	Farm or Lease Name: Payne
Csg. Size: 5 1/2 / Wt.: 17 & 15.5# / d: 4.950 / Set At: 6680			Perforations: From 6436 To 6545		Well No.: 3-E
Tbg. Size: 1 1/2 / Wt.: 2.76# / d: 1.610 / Set At: 6518			Perforations: From To		Unit: D / Sec.: 26 / Twp.: 31 / Rge.: 13
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: G - O			Packer Set At: 5935		County: San Juan
Producing Thru: Tbg	Reservoir Temp. °F: n	Mean Annual Temp. °F	Baro. Press. – P_a		State: New Mexico
L	H	Gg: .650 est.	% CO_2	% N_2	% H_2S
Prover: 6" pos.	Meter Run: choke	Taps			

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	Shut 14 days				1783		Pkr.		
1.					201	60	Pkr.		3 hrs.
2.									
3.									
4.									
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.00		213	1.000	1.240	1.022	2969.2
2							
3							
4							
5							

NO.	P_r	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1795 P_c^2 3222025

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		823.7	678.416	2543609
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2667$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1940$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3545.2$

Absolute Open Flow 3545.2 Mcfd @ 15.025 Angle of Slope θ 53.13 Slope, n .75

Remarks:

Approved By Division	Conducted By:	Calculated By:	Checked By: