

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7/27/84	
Company Union Texas Petroleum Corp.			Connection El Paso Natural Gas Company		
Pool Basin			Formation Dakota		
Completion Date 7/11/84		Total Depth 6545		Plug Back TD 6498	
				Elevation 5630	
Cng. Size 4.500		Wt. 10.50		Set At 6541	
Perforations: From 6292 To 6493		Well No. 1-E			
Tng. Size 2.375		Wt. 4.70		Set At 6304	
Perforations: From 6244 To 6250		Unit Sec. Twp. Rge. F 34 31N 13W			
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single				Packer Set At	
Producing Thru Tubing		Reservoir Temp. °F #		Mean Annual Temp. °F	
				Baro. Press. - P _a 12	
County San Juan		State New Mexico			
L 6232		H		G _g 0.700	
% CO ₂		% N ₂		% H ₂ S	
Prover		Meter Run		Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2		3/4"				1781		1801		7 days
1.							227	86°	885		3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.3650		237	0.9759	0.9258	1.023	2709
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _g	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1813 P _c ² 3,286,969				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		897	804,609	2,482,360
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.3241}{1.3241 - 0.897^2} = 1.3241$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.2343}{1.2343 - 0.897^2} = 1.2343$

LOG = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3344$

Absolute Open Flow	3344	Mcf @ 15.025	Angle of Slope	Slope, n	0.75
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Remarks:

Approved by Commission:	Conducted by: Floyd Woodward	Calculated by: Ken Roddy	Checked by:
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