OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 11/26/84	
Company: Union Texas Petroleum Corp.		Connection: Southern Union Gathering Company			
Pool: Basin		Formation: Dakota		Unit	
Completion Date: 10/3/84	Total Depth: 7010	Plug Back TD: 6835	Elevation: 5952	Farm or Lease Name: Senter Federal	
Csg. Size: 4.500	Wt.: 10.50 / 11.60	d: 4.052 / 4.000	Set At: 7009	Perforations: From 6716 To 6797	Well No.: 1-E
Tbg. Size: 1.900	Wt.: 2.90	d: 1.610	Set At: 6751	Perforations: Open-Ended From To	Unit: P; Sec.: 26; Twp.: 31N; Rge.: 13W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: NA		County: San Juan	
Producing Thru: Tubing	Reservoir Temp. °F: @	Mean Annual Temp. °F:	Baro. Press. – P_a: 12	State: New Mexico	

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
6744		0.650						

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	2"	3/4"				1405		1414		7 days
1.						95	56°	625		3 hours
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		107	1.0039	0.9608	1.000	1276
2.							
3							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1426 P_c^2 2,033,476

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		637	405,769	1,627,707
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2493$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1816$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1508$

Absolute Open Flow 1508 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n 0.75

Remarks: _____

Approved By Division	Conducted By:	Calculated By:	Checked By:
	Connie Clevenger	Ken Roddy	