

NEW MEXICO OIL CONSERVATION COMMISSION  
GAS WELL TEST DATA SHEET -- SAN JUAN BASIN

(To be used for Fruitland, Pictured Cliffs, Mesaverde, & all Dakota  
except Barker Dome Storage Area)

POOL Mesaverde FORMATION Mesaverde COUNTY San Juan

PURCHASING PIPELINE Southern Union Gathering System DATE TEST FILED July 28, 1960

OPERATOR Antee Oil & Gas Company LEASE Thompson WELL NO. 3  
 UNIT 3 SEC. 34 TWP. 31 RGE. 12 PAY ZONE: From 4735 To 5110  
 CASING: OD 5 WT. 15.5 SET AT 4737 TUBING: OD 2 WT. 1.7 T.Perf. 100%  
 PRODUCED THROUGH: CASING X TUBING X GAS GRAVITY: MEASURED .679 ESTIMATED .679  
 DATE OF FLOW TEST: From 5/21 To 6/7 \*Date S.I.P. MEASURED 6/14/60  
 METER RUN SIZE 4 ORIFICE SIZE 0.313 TYPE CHART 1 TYPE TAPS 2

OBSERVED DATA

Flowing casing pressure (Dwt) 533 psig + 12 = 545 psia (a)  
 Flowing tubing pressure (Dwt) 523 psig + 12 = 535 psia (b)  
 Flowing meter pressure (Dwt) 523 psig + 12 = 535 psia (c)  
 Flowing meter pressure (meter reading when Dwt. measurement taken:  
     Normal chart reading. . . . . psig + 12 = . . . . . psia (d)  
     Square root chart reading ( )<sup>2</sup> x spring constant = 523 psia (d)  
 Meter error (c) - (d) or (d) - (c). . . . . ± = plus 2 psi (e)  
 Friction loss, Flowing column to meter:  
     (b) - (c) Flow through tubing: (a) - (c) Flow through casing... = 0 psi (f)  
 Seven day average static meter pressure (from meter chart):  
     Normal chart average reading . . . . . 530 psig + 12 = 542 psia (g)  
     Square root chart average reading ( )<sup>2</sup> x sp. const. = 530 psia (g)  
 Corrected seven day avge. meter press. (p<sub>f</sub>) (g) + (e) = 530 psia (h)  
 P<sub>t</sub> = (h) + (f) . . . . . = 530 psia (i)  
 Wellhead casing shut-in pressure (Dwt) 738 psig + 12 = 750 psia (j)  
 Wellhead tubing shut-in pressure (Dwt) 730 psig + 12 = 742 psia (k)  
 P<sub>c</sub> = (j) or (k) whichever well flowed through. . . . . = 742 psia (l)  
 Flowing Temp. (Meter Run) . . . . . 75 °F + 460 . . . . . = 535 °Abs (m)  
 P<sub>d</sub> =  $\frac{1}{2}$  P<sub>c</sub> =  $\frac{1}{2}$  (l) . . . . . = 366 psia (n)

FLOW RATE CALCULATION

$$Q = \frac{36}{(\text{integrated})} \times \left( \frac{T(c)}{\sqrt{T(d)}} = \frac{(2.0038)^{0.5}}{2.0019} = 36 \right) = 36 \text{ MCF/da.}$$

DELIVERABILITY CALCULATION

$$D = Q \times \left[ \frac{\left( \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right)^{0.5}}{1.5947} \right] = \frac{36}{1.5947} = 23 \text{ MCF/da.}$$

SUMMARY

P <sub>c</sub> = <u>738</u>	psia	Company <u>Antee Oil &amp; Gas Company</u>
Q = <u>36</u>	Mcf/day	By <u>ORIGINAL SIGNED BY L. M. STEVENS</u>
P <sub>w</sub> = <u>530</u>	psia	Title <u>L. M. Stevens, Dist. Eng.</u>
P <sub>d</sub> = <u>366</u>	psia	Witnessed by _____
D = <u>23</u>	Mcf/day	Company _____

\* This is date of completion test.

\* Meter error correction factor

REMARKS OR FRICTION CALCULATIONS

GL	(1-e <sup>-s</sup> )	(F <sub>c</sub> Q)2	(F <sub>c</sub> Q) <sup>2</sup> R <sup>2</sup>	(1-e <sup>-s</sup> ) R <sup>2</sup>	P <sub>t</sub> <sup>2</sup> (Column 1)	P <sub>t</sub> <sup>2</sup> + R <sup>2</sup>	P <sub>w</sub>
Friction loss is variable							

