

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☒ Special				Test Date 4-5-84	
Company Amoco Production Company				Connection Gas Company of New Mexico	
Pool Ute Dome				Formation Dakota	
Completion Date 3-13-84		Total Depth 2385		Plug Back TD 2314	
				Elevation 6094 GL	
Csg. Size 6.250		Wt. 26		Set At 2385	
Perforations: From 2160		To 2236		Well No. #1	
Tub. Size 2.375		Wt. 4.7		Set At 2292	
Perforations: From Open		To Ended		Unit Sec. Twp. Rye. D 1 31 14	
Type Well - Single - Blindhead - G.C. or G.O. Multiple Single				Facker Set At None	
Producing Thru Tubing				County San Juan	
Reservoir Temp. °F #		Mean Annual Temp. °F		State New Mexico	
L	H	Gg	% CO ₂	% H ₂	% H ₂ S
Prover		Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	90Axs						323		323		
1.	2.375		.750				110		186		3 hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		122	1.000	.9258	1.014	1416
2.							
3.							
4.							
5.							

NO.	R	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/hbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ XXXXXXXXXX
3.					Specific Gravity Flowing Fluid _____ XXXXXX
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 335 P _c ² 112225			
NO.	P ₁ ²	P _w	P ₂ ²
1		198	39204
2.			
3.			
4.			
5.			

(1) $\frac{P_c^2}{P_1^2 - P_w^2} = 1.5369$		(2) $\left[\frac{P_c^2}{P_1^2 - P_w^2} \right]^n = 1.3803$	
AOF = Q $\left[\frac{P_1^2}{P_c^2 - P_w^2} \right]^n = 1955$			

Absolute Open Flow _____ 1955	Mcfd @ 15.025	Angle of Slope α _____	Slope, n _____ .75
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Re-frac	
Remarks: Flowed dry was not flared	

Approved By Division	Conducted By I. Bennett	Calculated By I. Bennett	Checked By
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