## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS
Revised 12-1-55

Poc	ol Blanco M	esaver	de	F	ormation Mesaverde				County San Juan				
Initial X Annual Special Date of Test 7-24-75													
Company Blackwood & Nichols Lease Northeast Blanco Unit Well No. 63													
Unit N Sec. 13 Twp. 30N Rge. 8W Purchaser El Paso Natural Gas Company													
Casing 4½" Wt. 10.50# I.D. 4.05 Set at 5605' Perf. 5185' To 5528'													
Tubing 2-3/8" Wt. 4.7# I.D. 1.995 Set at 5478' Perf. 5478' To 5478'													
Gas Pay: From 5185' To 5528' L 5478 xG .59 _GL 3232 Bar.Press. 12.0													
	Producing Thru: Casing Tubing X Type Well Gas  Single-Bradenhead-G. G. or G.O. Dual												
Dat	e of Complet	ione	7_10_	75	Paaka	n None	Sin	gle-Brade	nhead-G.	G. or (	G.O.	Dual	
Day	Date of Completion: 7-18-75 Packer None Reservoir Temp. 1480  OBSERVED DATA												
m	L	(D	<b>\</b>	a	(M. )		ED DATA		<b></b>				
Tested Through (Rrawer) (Choke) (Meter)  Type Taps													
	Flow D. (Prover) (Choke)				D:00				Casing Data		<b>⊣</b>		
No.		(Orif	ice)					Temp.	Press.			Duration of Flow	
SI	Size	Si	ze	psig	h <sub>w</sub>	° <sub>F</sub> .	psig	°F.		F.		Hr.	
1.		3/4	11	175			560 175		580 520	<del> </del>	<del> </del>	3 hrs.	
2.		<del> </del>		1/3	<del> </del>		1/3			<u> </u>	<del>                                     </del>	J HES.	
3.													
4.													
5.		<u> </u>		ļ	L						<u> </u>		
					1	FT.OW CAT	CULATION	5					
	Coeffici	ent		Pr			Temp.	Gravity Compress. Rate of Flow					
No.						Fac	tor	Factor	Factor		Q-MCFPD		
l	$(24-Hour)$ $\sqrt{h_v}$		$\sqrt{h_{w}}$	p <sub>f</sub> psia		F.	t	Fg	Fpv		@ 15.025 psia		
1. 2.	12.3650		<del></del>	187							2313		
2.													
3° 4° 5°	<del></del>												
4.													
-20-1	<del></del>												
					PRI	ESSURE CA	ALCULATIO	ONS					
	Liquid Hydro					cf/bbl.			fic Gravit				
	ity of Liquid	d Hydro	ocarbo / 1	ons L-e <sup>-s</sup> )		deg.			fic Gravit				
· c			\	L-e 2/_				<sup>P</sup> c	592	_Pc3	50464	<u>+</u>	
	$P_{\mathbf{w}}$	2					2		2 2			<u></u>	
No.	5 ( )	$P_{\mathbf{t}}^{2}$	F	,Q	$(F_cQ)^2$	(F	$(e^{Q})^2$	$P_w^2$	$P_c^2 - P_w^2$		1.	₽ <b>₩</b> ₽ <sub>C</sub>	
	Pt (psia)					(1.	-e <sup>-s</sup> )			P	w	F <sub>C</sub>	
1. 2.			+	<del></del>		<del>-                                    </del>	<del></del>			<del> </del>			
3.		<del></del>								<del> </del>	<del></del>		
3. 4.											<u> </u>		
5.													
Absolute Potential: 7955 MCFPD; n .75  COMPANY Blackwood & Nichols Company  ADDRESS P-O. Box 1237) Durango, Colorado 81301  AGENT and TITLE Delasso Loos, District Manager  WITNESSED REMARKS													
COME	PANYB1a	ckwood	l & Ni		Company	<u> </u>			JAY U	Jak .	15	1	
						orado 81			KA	4			
	T and TITLE	hte	Za	sso I	toe-DeI	asso Loc	s. Distr	ict Manag	er	1.0	COM	<b>1</b>	
COMP	TESSED				<del></del>				<del>-/-7</del> /	-0 <del>1</del>	3/	Z	
OOM	DMT			<del></del>		REM	ARKS		-/0	4 018)	1		

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure  $(P_W)$ . MCF/da. @ 15.025 psia and 60° F.
- P<sub>c</sub>= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw- Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt\_ Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- $h_{\mathbf{W}}^{-}$  Differential meter pressure, inches water.
- FgT Gravity correction factor.
- $F_{t}$  Flowing temperature correction factor.
- $F_{DV}$  Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If  $P_{\mathbf{W}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{W}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .